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# Safety and Design Improvements at Rural Expressway Median Crossovers (Phase 1) 



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# Safety and Design Improvements at Rural Expressway Median Crossovers (Phase I) 

# MISSOURI DEPARTMENT OF TRANSPORTATION RESEARCH, DEVELOPMENT AND TECHNOLOGY 

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The opinions, findings, and conclusions expressed in this publication are those of the principal investigators.

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## EXECUTIVE SUMMARY

Expressway medians provide a separation area between opposing lanes of traffic. Crossovers in medians provide protection and control for cross and turning traffic. The objective of this study was to provide a means for MoDOT engineers to determine whether particular highspeed rural expressway crossovers are performing satisfactorily and, if not, to assess alternatives for crossover design.

Design practices of other states were examined and alternative design options were identified. The Highway Capacity Manual (HCM) approach and the CORSIM simulation technique were compared to determine how best to identify appropriate alternatives. A procedure was then developed to assist MoDOT district traffic and design engineers in selecting improvements for existing crossovers as they become congested. That procedure is described directly below.

## RECOMMENDED PROCEDURE FOR SELECTING IMPROVEMENTS

1. Identify potential problems at Type II rural crossovers. It is expected that MoDOT Districts are aware of possible congestion and safety problems at their crossovers through their normal procedures of observation and through citizen comments.
2. Observe specific crossover during likely time periods of concern to identify congestion problems. If problems are observed, continue to step 3.
3. Examine list of potential alternative treatments (see Ch. 2). Identify feasible treatments and appropriate performance measures (see Ch. 3).
4. Apply CORSIM simulation tool to existing condition and to feasible treatments (see Ch. 4). Input data will include of geometric, operations, demand, and control data. Outputs will include performance measures to compare alternatives.
5. Estimate costs of treatments (see Ch. 6).
6. Identify best alternative, based upon selected performance measures.
7. Implement and monitor solution.

## INTRODUCTION

Expressway medians provide a separation area between opposing lanes of traffic. The normal purpose of a crossover is to provide access for crossing traffic, left-turning traffic, and U-turning movements. Crossovers in those medians provide protection and control for cross and turning traffic. MoDOT only considers Type-II median crossovers at State Routes, county roads, and major streets.

This report describes the results of the first phase of a study of rural median crossovers. The immediate following sections describe the objectives, present conditions, technical approach used. This is followed by a lengthy section describing results and conclusions.

Within the section on Results and Discussion, Chapter 1 describes introductory information. Chapter 2 describes a wide range of treatments that can be considered for crossovers experiencing or expected to experience congestion. Chapter 3 summarizes various performance measures (measures of effectiveness) that a MoDOT engineer might wish to use in examining the alternatives for improvement. Chapter 4 provides a description of how to apply the CORSIM model to simulate crossovers and examine improvement strategies. Similarly, Chapter 5 describes the HCM approach and why it was found to be a inferior to CORSIM for analyzing the problem of rural crossovers. Chapter 6 provides information on estimating costs. Appendix 1 provides a summary of some of the research and design literature relevant to the problem of rural crossovers. Appendix 2 summarizes recent state design, operations and safety experience. Appendix 3 provides information about crossovers of concern to MoDOT Districts.

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## Introduction

Expressway medians provide a separation area between opposing lanes of traffic. The normal purpose of a crossover is to provide access for crossing traffic, left-turning traffic, and U-turning movements. Crossovers in those medians provide protection and control for cross and turning traffic. MoDOT only considers Type-II median crossovers at State Routes, county roads, and major streets.

This report describes the results of the first phase of a study of rural median crossovers. The immediate following sections describe the objectives, present conditions, technical approach used. This is followed by a lengthy section describing results and conclusions.

Within the section on Results and Discussion, Chapter 1 describes introductory information. Chapter 2 describes a wide range of treatments that can be considered for crossovers experiencing or expected to experience congestion. Chapter 3 summarizes various performance measures (measures of effectiveness) that a MoDOT engineer might wish to use in examining the alternatives for improvement. Chapter 4 provides a description of how to apply the CORSIM model to simulate crossovers and examine improvement strategies. Similarly, Chapter 5 describes the HCM approach and why it was found to be a inferior to CORSIM for analyzing the problem of rural crossovers. Chapter 6 provides information on estimating costs. Appendix 1 provides a summary of some of the research and design literature relevant to the problem of rural crossovers. Appendix 2 summarizes recent state design, operations and safety experience. Appendix 3 provides information about crossovers of concern to MoDOT Districts.

## Objective

The objective of this study was to provide a means for MoDOT engineers to determine whether particular high-speed rural expressway crossovers are performing satisfactorily and, if not, to assess alternatives for crossover design.

## Present Conditions

MoDOT only considers Type-II median crossovers at State Routes, county roads, and major streets. There is currently no procedure to determine the conditions under which alternative treatments should be considered.

## Technical Approach

The design practices of other states were examined, as well as design alternatives that have been suggested in traffic and highway design references. Two alternative tools to evaluate potential improvements, the Highway Capacity Manual ${ }^{3}$ (HCM) approach and the CORSIM simulation technique, were compared to determine how best to identify appropriate alternatives. A procedure was then developed to assist MoDOT district traffic and design engineers in selecting improvements for existing crossovers as they become congested with increasing crossing and left turn movements. Phase II of this study will provide further useful information from an extensive field study of existing crossovers.

## Results and Discussion

## I. INTRODUCTION

As described in the Missouri Department of Transportation's (MoDOT's) Policy, Procedure and Design Manual ${ }^{1}$, expressway medians provide a separation area between opposing lanes of traffic. Crossovers in those medians provide protection and control for cross and turning traffic. MoDOT only considers Type-II median crossovers at State Routes, county roads, and major streets. A simplistic sketch of a Type-II median crossover is shown in Figure 1-1. Detailed sketches are available in MoDOT's design manual and through its web site ${ }^{2}$.


Figure 1-1: Type II Median Crossover
The normal purpose of a crossover is to provide access for crossing traffic, left-turning traffic, and U-turning movements. Each of these three movements can be complex for the following reasons:

- While the expressway speed is high, speeds of crossing and turning vehicles are low.
- The lengths and required turning paths of the various design vehicles making these movements must be accommodated within the median width.
- Crossing, left-turning, and U-turning drivers must find gaps in conflicting traffic before they leave the crossover.
- The presence of other waiting vehicles can block a driver's view of conflicting traffic.
- The combination of crossing, left-turning, and U-turning traffic and the conflicting traffic to which these movements must yield can lead to a situation in which through lanes of the expressway may be blocked.

The objective of this study was to provide a means for MoDOT engineers to determine whether particular high-speed rural expressway crossovers are performing satisfactorily and, if not, to assess alternatives for crossover design.

The design practices of other states were examined, as well as design alternatives that have been suggested in traffic and highway design references. Two alternative tools to evaluate potential improvements, the Highway Capacity Manual ${ }^{3}$ (HCM) approach and the CORSIM simulation technique, were compared to determine how best to identify appropriate alternatives. A procedure was then developed to assist MoDOT district traffic and design engineers in selecting improvements for existing crossovers as they become congested with increasing crossing and left turn movements. That procedure is described directly below.

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7. Implement and monitor solution.

## ORGANIZATION OF THIS section

Chapter 2 describes a wide range of treatments that can be considered for crossovers experiencing or expected to experience congestion. Chapter 3 summarizes various performance measures (measures of effectiveness) that a MoDOT engineer might wish to use in examining the alternatives for improvement. Chapter 4 provides a description of how to apply the CORSIM model to simulate crossovers and examine improvement strategies. Similarly, Chapter 5 describes the HCM approach and why it was found to be inferior to CORSIM for analyzing the problem of rural crossovers. Chapter 6 provides information on estimating costs.

Appendix 1 provides a summary of some of the research and design literature relevant to the problem of rural crossovers. Appendix 2 summarizes recent state design, operations and safety experience. Appendix 3 provides information about crossovers of concern to MoDOT Districts.

## II. ALTERNATIVE TREATMENTS TO ADDRESS PROBLEMS

There are several kinds of problems related to the Type II median crossover. NCHRP Synthesis 281: Operational Impacts of Median Width on Larger Vehicles ${ }^{4}$ and NCHRP Report 375: Median Intersection Design ${ }^{5}$ provide comprehensive analyses of median opening operations for urban, suburban, and rural highways. The rural highways problems and alternative treatments applicable to Type II median crossovers described in these reports are summarized below. The identified problems are ${ }^{4}$ :

1. Undesirable driving behavior, including:

- Encroachment on through lanes by vehicles in the median opening,
- Side-by-side queuing in the median opening, and
- Angle stopping in the median opening.

2. Collisions between left-turning vehicles and vehicles stopped in the median opening.
3. Collisions between vehicles turning left from the divided highway and other same-direction vehicles.
4. Collisions between vehicles turning left from the divided highway and opposing through vehicles.
5. Collisions between vehicles making U-turns and opposing through vehicles.

The task of choosing particular mitigation techniques is based on the types of collisions to be prevented. Mitigation techniques, described in NCHRP Synthesis $281^{4}$ and NCHRP Report $375^{5}$, for each of the above five problem types are described below. The reader is referred to the above references for more detailed discussion of specific measures.

## Undesirable Driving Behavior and Collisions Involving Vehicles in the Median Opening Area

(1) Reconstruct rural highways with wider median.

The width of median should be able to store safely at least one of the largest vehicles using the intersection most often. In some cases, several vehicles may need to be stored. The width of the median should not attract an additional vehicle to enter if the added vehicle would encroach on the through lanes.
(2) Prohibit left-turn maneuvers.
(3) Close median opening.
(4) Reconfigure median to prohibit crossing maneuvers while still permitting left turns.

For the above three techniques, consideration must be given to the alternate routes that will be used by the diverted traffic and the traffic operational and safety impacts on other locations.
(5) Provide median acceleration lanes.

It was indicated by NCHRP Report $375^{5}$ that, on the basis of the guidelines used by state highway agencies, acceleration lanes for left-turning vehicles from a crossroad onto the divided highway should be considered at locations where adequate median width is available and:
(a) limited gaps are present in the major-road traffic;
(b) the low-speed turning traffic merges with high-speed through traffic;
(c) rear-end or sideswipe accidents crashes are prevalent;
(d) required intersection sight distance is not present; and
(e) there are high volumes of trucks turning into the divided highway from the median opening.
(6) Extend edgelines to better define median opening area.
(7) Mark double yellow centerline on roadway in the median opening to discourage angle stopping.
(8) Remove STOP signs in median. NCHRP Report $375{ }^{5}$ states that most highway agencies use no control in the median opening area for median widths up to 9 m (30ft). Most use YIELD control for median widths from 9 to 25 m ( 30 to 82 ft ). Most use STOP control for median widths greater than 25 m ( 82 ft ).
(9) Install traffic signals. Traffic signals are seldom used in rural areas. Traffic signals at median openings should be considered only when the signal warrants of the Manual on Uniform Traffic Control Devices ${ }^{6}$ are met ${ }^{4}$.

## Collision Between Vehicles Turning Left from the Divided Highway and Other Same-Direction Vehicles

These collisions are often caused by turning conflicts that are not expected by through motorists on the divided highway. The large speed differences between the turning and thorough vehicles contribute to crash frequency and severity ${ }^{4}$. Mitigation techniques include:
(1) Install advance intersection signing.

Intersection advance warning sign or advance guide signs, with the name of the intersecting road, or both, can be used ${ }^{4}$.
(2) Install bigger signs.
(3) Install better delineation.

This method can include:
(a) marking channelizing islands with reflective paint,
(b) creating obvious breaks in delineator spacing at the crossover, and
(c) creating obvious breaks in pavement markings at the crossover ${ }^{4}$.
(4) Implement lower speed limits.

A speed limit change should only be considered on the basis of an engineering study ${ }^{6}$.
(5) Implement advisory speeds on major road ${ }^{4}$.
(6) Increase the deceleration and storage length of existing left-turn lanes.

AASHTO gives guidance on lengths for left-turn lanes, based upon the appropriate distances for deceleration and storage ${ }^{7}$.
(7) Prohibit left turns from the major road.
(8) Close the median opening.

Alternate routes must be considered for the last two options.

## Collisions between Vehicles Turning Left and Opposing Through Vehicles

Limited sight distance is the primary cause of this kind of problems. Mitigation techniques include:
(1) Prohibit left turns from the major road.
(2) Close the median opening.

Consideration must be given to the alternate routes for both of these options.

Collisions Between Vehicles Making U-Turns and Opposing through Vehicles

U-turn maneuvers have potentially higher safety risks than comparable left-turn maneuvers. Mitigation techniques for the accident pattern involving U-turn collisions include:
(1) Increase width of paved/stabilized shoulder to allow trucks to swing wider.
(2) Reconstruct highway with wider median or reconstruct at selected intersections.
(3) Provide a different median crossover or indirect routes for U-turns.
(4) Prohibit U-turn maneuver or U-turn maneuvers by larger vehicles.
(5) Close the median opening.

Consideration must be given to the alternate routes for these options.

NCHRP Synthesis $281^{4}$ indicates many highway agencies have problems with medians that are too narrow. While only some of these medians would serve the same purposes as Type II median crossovers, Table 2-1 is included below to show use of some general countermeasures to address problems.

TABLE 2-1: HIGHWAY AGENCY USE OF SPECIFIC MITIGATION MEASURES FOR TRAFFIC OPERATIONAL PROBLEMS RELATED TO LARGER VEHICLES AND NARROW MEDIANS ${ }^{4}$

| Mitigation Measures | Agencies Using <br> This Measure* |
| :--- | :--- |
| Reconstruct highway with wider median | $4(15.4)$ |
| Reconstruct highway with wider median only at selected intersections | $7(26.9)$ |
| Provide left-turn lanes | $19(73.1)$ |
| Prohibit left turns | $9(34.6)$ |
| Close median opening | $15(57.7)$ |
| Reconfigure median to prohibit crossing maneuvers while still permitting left turns | $6(23.1)$ |
| Provide median U-turn roadways | $4(15.4)$ |
| Provide median acceleration lanes | $7(26.9)$ |
| Improve signal timing at adjacent signals | $11(42.3)$ |

* Percentages (shown in parentheses) are based on the total of 26 highway agencies that report traffic operational and safety problems related to larger vehicles and narrow medians.


## III. ALTERNATIVE PERFORMANCE MEASURES

The performance measures most often used to analyze intersection operations are volume-to-capacity ratio, delay, level of service, queue length, fuel consumption, and stops. For the specific problem of congested rural Type II crossovers, another important performance measure is the proportion of time a through lane on the expressway is blocked (closely related to queue length) by vehicles waiting to use the crossover.

The tools examined in this report are simulation, through the NETSIM program within CORSIM ${ }^{8}$, and the Highway Capacity Manual ${ }^{3}(\mathrm{HCM})$, as applied through the Highway Capacity Software ${ }^{9}(\mathrm{HCS})$. The ability of each of these two approaches to provide relevant performance measures is presented below.

## CORSIM PERFORMANCE MEASURES

The CORSIM program provides a range of performance measures, based upon a summary of traffic conditions present during its simulation runs. There are two different ways to view the output. One option is to view an animation of the simulation. This can be useful in identifying obvious traffic problems that would result from a particular design.

The other option is to view tables and graphs summarizing results. This latter option can prove useful in evaluating alternatives quantitatively. CORSIM provides the following system-wide measures of effectiveness:

- Average total delay (vehicle-minutes)
- Average delay per vehicle (seconds)
- Average percent stops
- Average queue length
- Average maximum queue length
- Average fuel consumption (gallons)
- Average fuel consumption (mpg)
- Total Emissions of HC (grams/mile)
- Total Emissions of CO (grams/mile)
- Total Emissions of NO (grams/mile)

CORSIM can also describe for each link:

- Time spent moving
- Time spent stopped
- Average queue by lane
- Maximum queue by lane
- Number of lane changes
- Average vehicle occupancy

Importantly, CORSIM allows one to place a simulated detector at a location of interest. Since it is desirable that median crossover traffic not block expressway through lanes, an obvious location for detectors is in the through lanes at the crossover.

## HCM/HCS PERFORMANCE MEASURES

The HCM (and HCS) provides a smaller number of measures, based upon the expected average flow conditions predicted from its analytical approach. The principle measures output by the HCS program are average control delay (in seconds) and the level of service resulting from that average delay. The HCS output can be manually manipulated to estimate average queue length and maximum (actually $95^{\text {th }}$ percentile) queue length. In theory, one should be able to determine the maximum queue length expected in the crossover. However, as described in Chapter 5, the researchers were unable to adapt the HCS to provide that desired result.

## RECOMMENDED PERFORMANCE MEASURES

A principle performance measure should be the proportion of time a through lane on the expressway is blocked (closely related to queue length) by vehicles waiting to use the crossover. It would also be desirable to provide the performance measures estimated by CORSIM for use as additional measures of effectiveness.

## IV. USING SIMULATION TO EVALUATE ALTERNATIVES

Simulation models are often used to augment Highway Capacity Manual ${ }^{3}$ (HCM) results or in some cases to address issues that cannot be effectively resolved using the Manual. Existing tools for the analysis of highway operations contained in the HCM are based upon deterministic models that simply execute known relations efficiently ${ }^{10}$. In many situations this approach works well. In others, where there exist significant random components, such as vehicle arrivals and queuing, a stochastic approach may be more efficacious. Interrupted flow simulation models, such as CORSIM ${ }^{8}$, attempt to incorporate randomness in a system explicitly. They use traditional statistical techniques to represent complex systems thus allowing inferences to be made about system behaviour. These types of models have many strengths. They allow:

- Explicit treatment of the randomness which is innate to the crossover situation,
- Study of the effects of changes on the operation of a system,
- Experimenting with new situations that do not currently exist,
- Modeling of queuing processes.

Other features relevant to rural crossovers, which are currently not available in the HCM but which CORSIM provides, are ${ }^{11}$ :

- Oversaturated conditions
- Bus and truck activity
- Special lane use
- Geometrically offset intersections
- Explicit actuated control
- Alternating arrival characteristics
- Two stage gap acceptance - especially applicable for analysis of rural crossovers

CORSIM is a microscopic simulation model for an integrated urban network freeway network, or corridor analysis. CORSIM consists of FRESIM, a microscopic model of freeway traffic, and NETSIM, a microscopic model of urban streets, as well as a traffic assignment model. CORSIM was chosen for this study for several reasons. It was developed for the Federal Highway Administration, has many qualities that recommend its use, as described later, and is commonly used in the industry and is the software of choice at MoDOT.

As indicated in previous sections of this report, rural expressway facilities can generate hazardous crossing situations and confusing vehicle operations at rural median crossovers. As volumes increase through a crossover area, multiple vehicles can be positioned in the median so they actually block each other and impede visibility to oncoming vehicles. The AASHTO Green Book ${ }^{7}$ does not provide a complete solution to the problem. No guidance is provided on how to solve the problem of crossing vehicles stacking up in the median area, or the hazard that can be created by long vehicles protruding into the through lane. Further, AASHTO does not provide a solution for those crossovers which have been placed in a median that is narrower than 60 feet. The purpose of this chapter is to explain the use of simulation software, which may be used to address these issues, for evaluating alternative rural crossover designs.

Five designs were chosen as illustrative of what may be used in Missouri. They are depicted in Figure 4.1. The CORSIM software was used to evaluate two of these configurations for two different operational and control situations described later. This exercise provides information about the use of simulation software for this purpose. The information will be used in the following pages to evaluate that use.

## INPUT REQUIREMENTS

There exist four general categories of inputs and outputs: geometrics, operations, demand and control. Geometrics describe the physical network over which vehicles travel. Details include number of lanes, turn bays, lane lengths, lane use and grade as well as topology. CORSIM uses the link-node concept to represent networks where a link represents a road section and a node represents either an intersection or a change in road geometry. Creation of the five alternative cases as shown in Figure 4.1 required approximately 45 minutes to one hour each. Operational data are link specific - for example, capacities, lane use, lane restrictions, free flow speed, HOV lanes, parking, lane blockages, and so on.

Demand data may be entered in two different ways in CORSIM, either by using O-D data at the entrance and exit points of the network with turn proportions specified at intersections, or by entering explicit volumes on links and turn volumes at intersections. Up to sixteen different time periods may be defined which are used to divide the simulation into periods of similar character such as pre-peak hour, peak hour and post peak hour. Control data include the full array of signage and signals. Entry of volume data requires fairly significant manipulation in order to put it into a useful form. Total time per site took about 1 hour which includes data entry and reduction, and reallocating volumes under the alternative scenarios (these would need to be done regardless of tool used). Schematic drawings of the two alternatives are provided in Figure 4.2.

The TRAF suite of software includes a graphical interface, called ITRAF, a simulation algorithm called CORSIM and a graphics generator called TRAFVU. ITRAF allows creation of a transportation system relatively quickly and easily along with the entry of the other data types, and TRAFVU provides animation of individual runs in addition to more familiar modes of data output as described below. TRAF
is a Windows-based software and provides very useful features that are common to this type of software, namely, button-pad commands, on-line help facility, of course all menu driven, point and click inputs for nodes and links in a network. It also allows a great deal of flexibility in the choices of other variables to use. For example, the user may specify volumes entering the system with turn percentages at intersections, or he/she may enter turn volumes explicitly at intersections. Lanes may be designated as being blocked if one has interest in the effects of incidents on traffic.
(insert Fig. 4.1 here)
(Insert Fig 4.2a Schematics of Existing Conditions here)
(insert Figure 4.2b. Schematics of Improved Conditions here)

## PERFORMANCE MEASURES

Outputs from simulation are provided in two very different forms. The user may opt to view an animation of the actual implementation of his/her designs using specified geometrics, operation and control information. This form of output allows one to identify gross problems with the intersection. It provides an excellent means to eliminate problem configurations very quickly and to view alternative scenarios also very quickly. The second form of output is the more familiar tables and graphics. This, for analytical purposes is far superior. Tables 4.1 through 4.4 (shown at the end of this Chapter) provide a sample listing of outputs obtained from CORSIM. These numerical outputs are crucial for assessing alternatives quantitatively. Additionally, for each link a table or graph may be generated which tracks a variable of interest over time - see Figure 4.3. As the Tables show, the software can be used to model all of the five design options quite precisely.
(Insert Figure 4.3 Time Plot of Total Vehicle Delay here)

## CASE STUDIES

Data for six type II median crossovers were obtained from MoDOT District 8. The two sites selected for analysis are Route 13 at Route O and Route 160 at Farm Road 157 both in Greene County. The sites were examined under existing conditions and under one alternative geometry - case 3 depicted in Figure 4.1. Case 3 was chosen due to its simplicity and for its relative low cost (see Chapter 6).

Route 13 is a 4 lane divided highway with 12 foot lanes, 6 foot inside shoulders, 10 foot outside shoulders and a 60 foot median. There are no traffic signals at or near this location. Route 160 has the same geometrics as Route 13 except for a 40 foot median. Data from the two locations were entered into the TRAF software via ITRAF and were used to simulate operation at the sites. For the purpose of illustrating the use of simulation software, each site's existing conditions and one alternative design were examined. Simulation outputs allow both link-specific and system-level assessments. Both are useful in evaluating alternatives. With regard to the former, the output tables were used to identify problem links at the sites under existing conditions. Key performance measures were then compared for the two alternatives: existing versus case 3 . Table 4.5 depicts the comparisons. Table 4.6 compares selected system-wide outputs as well for each scenario. As both tables illustrate quite dramatically, the alternative design significantly improves most measures. The prime exception is fuel consumed which makes sense given the requirement for vehicles to travel further to navigate through the intersection. The gains in delay reductions, decreased queue lengths (with potentially lowered conflicts) and emissions levels all recommend the alternative design.

## EVALUATION

When evaluating software it becomes necessary to establish its operating goals. What features do we want it to have and what do we want it to be able to do? Features that are desirable for simulation software as it is applied here include accuracy and ease of use - both of which are discussed in detail in the paragraphs that follow. It should be noted that these features are often product specific. With regard to the second question, as always, one has interest in safety and efficiency. Efficiency measures include individual delay, queue length, fuel consumption and emissions. CORSIM provides all of these, as Tables 4.1 to 4.4 show. With regard to safety, CORSIM is similar to the HCM in its lack of safety outputs. However, the wide variety and very detailed operational outputs allow for more accurate assessments of safety.

## Accuracy and Precision of the Model

There are two sources at issue here: assumptions that must be made (and their accuracy as they pertain to rural crossovers), and the limitations of the tool selected. Since CORSIM is a stochastic model, it is assumed to be as random as the real world. Consequently, its resulting performance measures are samples from a population. That is, each measure is a random variable with a mean and variance. Several runs for a given situation are therefore needed. For a specified confidence level, a considerable number of runs may be necessary. In addition to confidence level, the number depends upon the variable of interest, its variance and its required precision. For example, if queue length were the variable of interest, assuming a variance of 4 and a required precision of 1 vehicle, the required number of runs would be around 16 . The appropriate number of runs derives from specification of a time interval duration which is used to control the requirements for frequency of output in CORSIM. An appropriate interval must be assumed since the variance of each variable is not known a priori.

Other notable limitations of the software include its inability to accept separate lane width for median turn lanes. Thus, all lanes on a link must have the same width (e.g. left turn bays must be 12 feet in this case); enter median acceleration lanes; specify link lengths less than 50 feet. While this last means the software would not be directly usable for median widths of 50 feet or less, the software does give queue lengths and so could be used even for narrow medians for this purpose.

## Ease of Use

Elefteriadou et al. ${ }^{11}$ established two criteria for assessing the ease of use of a simulation model, namely how the software handles input data (preprocessing) and how it presents results (post processing).

The preprocessor, or input unit, used by the TRAF software package, as stated previously, is ITRAF. It is a windows-based graphical user interface akin to a geographic information system style of entry. It allows both graphical and numerical input of node and link positions, topology, and characteristics via a map of the network and a series of dialogs. This of course is a subjective evaluation but the software is fairly friendly. Indeed, it required a graduate student with fairly recent knowledge of the software only 15 minutes to enter all geometric data for each of the 5 configurations described before. Subsequent input, essentially to revise volumes and some geometrics, requires perhaps 5 minutes on average.

The postprocessor or output unit which generates files for subsequent analysis is the CORSIM component. CORSIM processes the input data from ITRAF and generates text output files with all of the variables listed in Tables 4.1 through 4.5. This may then be viewed using the TRAFVU module which allows tabular and graphical displays of the output data. The module also uses the output to simulate the operation of the network in a graphical display. A "run" requires approximately 5 minutes. Generation of graphics is fairly interactive, although the software is somewhat cumbersome in this regard.

## CONCLUSIONS

Simulation software addresses several problems, listed in this report, that cannot be addressed by the HCM model. It allows detailed analysis of wide medians and two stage gap acceptance situations. It provides very detailed estimates of expected queue lengths and other critical performance measures that are not provided by the HCM - in addition to delay measures, which are provided by both tools. Further, it is stochastic in nature and therefore thought to be more appropriate for this type of analysis. Given the relative low level of time required to use the software, its appropriateness for this application, its relative ease of use, minimal data requirements, high levels of precision, and the richness of its outputs, the simulation software seems an excellent tool for evaluating rural crossover alternatives.

Table 4.1a: Site 1 Delay Measures

| ExISTING | VEHICLE |  | VEHICLE MINUTES |  |  | $\begin{array}{\|l\|} \hline \text { RATIO } \\ \hline \text { MOVE/ } \\ \text { TOTAL } \\ \hline \end{array}$ | MINUTES/MILE |  | SECONDS/VEHICLE |  |  | AVERAGE VALUES |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | MOVE | DELAY | TOTAL |  | TOTAL | DELAY | TOTAL | DELAY | QUEUE* | STOP* | STOPS | VOLUME | SPEED |
| LINK | MILES | TRIPS | TIME | TIME | TIME |  | TIME | TIME | TIME | TIME | TIME | TIME | (\%) | VPH | MPH |
| (8001,1) |  | 398.0 |  |  |  |  |  |  |  |  |  |  |  | 398.0 |  |
| ( 1,5) | 149.2 | 394.0 | 138.2 | 13.7 | 151.9 | 0.9 | 1.0 | 0.1 | 34.6 | 13.6 | 11.8 | 11.8 | 4.0 | 394.0 | 58.9 |
| $(5,3)$ | 151.5 | 400.0 | 140.4 | 7.8 | 148.2 | 1.0 | 1.0 | 0.1 | 22.2 | 1.2 | - | - | - | 400.0 | 61.3 |
| $(8006,4)$ |  | 1,932.0 |  |  |  |  |  |  |  |  |  |  |  | 1,932.0 |  |
| $(4,6)$ | 702.3 | 1,854.0 | 650.5 | 1,340.9 | 1,991.4 | 0.3 | 2.8 | 1.9 | 109.7 | 89.0 | 69.1 | 64.7 | 27.0 | 1,854.0 | 21.2 |
| $(6,2)$ | 685.2 | 1,809.0 | 634.7 | 110.3 | 745.0 | 0.9 | 1.1 | 0.2 | 24.6 | 3.6 | - | - | - | 1,809.0 | 55.2 |
| $(8002,7)$ |  | 92.0 |  |  |  |  |  |  |  |  |  |  |  | 92.0 |  |
| ( 7,5) | 3.7 | 13.0 | 4.9 | 5.8 | 10.7 | 0.5 | 2.9 | 1.6 | 1,422.4 | 1,409.7 | 1,404.2 | 1,403.7 | 100.0 | 13.0 | 20.7 |
| ( 5,7) | 9.6 | 34.0 | 12.8 | 2.2 | 15.0 | 0.9 | 1.6 | 0.2 | 26.5 | 3.9 | 0.1 | 0.1 | - | 34.0 | 38.4 |
| $(5,6)$ | 0.1 | 7.0 | 0.1 | 8.3 | 8.4 | 0.0 | 126.0 | 124.6 | 846.6 | 846.1 | 837.6 | 836.5 | 85.0 | 7.0 | 0.5 |
| $(6,5)$ | 0.3 | 32.0 | 0.4 | 3.2 | 3.7 | 0.1 | 12.1 | 10.7 | 173.6 | 172.8 | 171.1 | 170.4 | 40.0 | 32.0 | 5.0 |
| ( 6,8) | 11.9 | 44.0 | 15.9 | 2.1 | 18.0 | 0.9 | 1.5 | 0.2 | 24.5 | 2.9 | - | - | - | 44.0 | 39.7 |
| ( 8,6) | 7.9 | 29.0 | 10.5 | 31.0 | 41.6 | 0.3 | 5.3 | 3.9 | 1,231.3 | 1,217.6 | 1,211.8 | 1,210.8 | 100.0 | 29.0 | 11.4 |
| (8004,8) |  | 102.0 |  |  |  |  |  |  |  |  |  |  |  | 102.0 |  |


| CASE 3 |  |  | VEHICLE MINUTES |  |  | $\begin{array}{\|l\|} \hline \text { RATIO } \\ \hline \text { MOVE/ } \\ \text { TOTAL } \\ \hline \end{array}$ | MINUTES/MILE |  | SECONDS/VEHICLE |  |  | AVERAGE VALUES |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | VEHICLE |  | $\begin{aligned} & \hline \text { MOVE } \\ & \text { TIME } \end{aligned}$ | DELAY <br> TIME | $\begin{gathered} \hline \text { TOTAL } \\ \text { TIME } \\ \hline \end{gathered}$ |  | TOTAL TIME | DELAY <br> TIME | $\begin{gathered} \hline \text { TOTAL } \\ \text { TIME } \\ \hline \end{gathered}$ | DELAY TIME | QUEUE* <br> TIME | $\begin{gathered} \hline \text { STOP* } \\ \text { TIME } \\ \hline \end{gathered}$ | STOPS <br> (\%) | $\begin{gathered} \hline \text { VOLUME } \\ \text { VPH } \\ \hline \end{gathered}$ | $\begin{array}{\|c} \hline \text { SPEED } \\ \text { MPH } \\ \hline \end{array}$ |
| LINK | MILES | TRIPS |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $(8001,1)$ |  | 398.0 |  |  |  |  |  |  |  |  |  |  |  | 398.0 |  |
| $(1,3)$ | 188.0 | 397.0 | 174.1 | 4.4 | 178.5 | 1.0 | 1.0 | 0.0 | 26.8 | 0.7 | - | - | 1.0 | 397.0 | 63.2 |
| $(3,5)$ | 144.3 | 508.0 | 133.7 | 39.8 | 173.5 | 0.8 | 1.2 | 0.3 | 20.5 | 4.7 | 0.8 | 0.7 | 7.0 | 508.0 | 49.9 |
| $(5,7)$ | 125.9 | 443.0 | 116.6 | 19.7 | 136.3 | 0.9 | 1.1 | 0.2 | 18.4 | 2.7 | 0.1 | - | - | 443.0 | 55.4 |
| $(7,9)$ | 192.7 | 407.0 | 178.5 | 4.6 | 183.1 | 1.0 | 1.0 | 0.0 | 27.0 | 0.7 | - | - | - | 407.0 | 63.1 |
| (8004,10) |  | 1,932.0 |  |  |  |  |  |  |  |  |  |  |  | 1,932.0 |  |
| $(10,8)$ | 915.7 | 1,934.0 | 848.2 | 52.6 | 900.9 | 0.9 | 1.0 | 0.1 | 27.8 | 1.6 | - | - | - | 1,934.0 | 61.0 |
| $(8,6)$ | 561.1 | 1,975.0 | 519.7 | 88.4 | 608.1 | 0.9 | 1.1 | 0.2 | 18.4 | 2.7 | 0.2 | 0.2 | 3.0 | 1,975.0 | 55.4 |
| $(6,4)$ | 576.4 | 2,029.0 | 533.9 | 108.8 | 642.7 | 0.8 | 1.1 | 0.2 | 18.9 | 3.2 | - | - | - | 2,029.0 | 53.8 |
| $(4,2)$ | 911.9 | 1,926.0 | 844.7 | 109.1 | 953.8 | 0.9 | 1.1 | 0.1 | 29.7 | 3.4 | - | - | - | 1,926.0 | 57.4 |
| $(4,3)$ | 1.3 | 111.0 | 2.5 | 1.6 | 4.1 | 0.6 | 3.3 | 1.3 | 2.2 | 0.9 | 1.1 | 1.0 | 25.0 | 111.0 | 18.5 |
| $(7,8)$ | 0.4 | 39.0 | 0.9 | 23.5 | 24.4 | 0.0 | 54.9 | 52.9 | 37.5 | 36.1 | 34.7 | 34.5 | 92.0 | 39.0 | 1.1 |
| $(8005,11)$ |  | 123.0 |  |  |  |  |  |  |  |  |  |  |  | 123.0 |  |
| $(11,6)$ | 45.2 | 123.0 | 60.3 | 33.5 | 93.7 | 0.6 | 2.1 | 0.7 | 45.2 | 16.1 | 11.1 | 10.9 | 100.0 | 123.0 | 28.9 |
| $(6,11)$ | 29.8 | 81.0 | 39.7 | 5.3 | 45.0 | 0.9 | 1.5 | 0.2 | 33.3 | 3.9 | 0.1 | - | - | 81.0 | 39.7 |
| $(6,5)$ | 0.3 | 26.0 | 0.4 | 8.2 | 8.6 | 0.1 | 29.1 | 27.8 | 19.8 | 18.9 | 17.2 | 15.5 | 34.0 | 26.0 | 2.1 |
| $(5,6)$ | 0.4 | 39.0 | 0.6 | 28.8 | 29.4 | 0.0 | 66.3 | 65.0 | 44.5 | 43.6 | 43.5 | 42.0 | 84.0 | 39.0 | 0.9 |
| $(5,12)$ | 58.0 | 153.0 | 77.3 | 9.8 | 87.1 | 0.9 | 1.5 | 0.2 | 34.0 | 3.8 | 0.1 | - | - | 153.0 | 39.9 |
| ( 12,5) | 37.5 | 99.0 | 50.0 | 15.9 | 65.9 | 0.8 | 1.8 | 0.4 | 39.5 | 9.5 | 4.1 | 3.9 | 100.0 | 99.0 | 34.2 |
| $(8006,12)$ |  | 98.0 |  |  |  |  |  |  |  |  |  |  |  | 98.0 |  |
|  | 3,788.9 | 2,567.0 | 59.7 | 9.2 | 68.9 | 0.9 | 1.1 | 0.2 | 1.6 | 0.2 | 0.0 | 0.0 | 16.9 |  | 55.0 |

Table 4.1b: Site 2 Delay Measures

| EXISTING | VEHICLE |  | VEHICLE MINUTES |  |  | $\begin{aligned} & \hline \text { RATIO } \\ & \hline \text { MOVE/ } \\ & \text { TOTAL } \end{aligned}$ | MINUTES/MILE |  | SECONDS/VEHICLE |  |  | AVERAGE VALUES |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\begin{array}{\|c\|} \hline \text { MOVE } \\ \text { TIME } \\ \hline \end{array}$ | DELAY <br> TIME | TOTAL <br> TIME |  | $\begin{array}{\|c\|} \hline \text { TOTAL } \\ \text { TIME } \\ \hline \end{array}$ | DELAY TIME | $\begin{aligned} & \text { TOTAL } \\ & \text { TIME } \end{aligned}$ | DELAY <br> TIME | QUEUE* | $\begin{gathered} \hline \text { STOP* } \\ \text { TIME } \end{gathered}$ | $\begin{gathered} \text { STOPS } \\ (\%) \end{gathered}$ | $\begin{gathered} \hline \text { VOLUME } \\ \text { VPH } \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { SPEED } \\ \text { MPH } \\ \hline \end{gathered}$ |
| LINK | MILES | TRIPS |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $(8001,1)$ |  | 1,681.0 |  |  |  |  |  |  |  |  |  |  |  | 1,681.0 |  |
| $(1,5)$ | 611.7 | 1,615.0 | 566.7 | 623.0 | 1,189.6 | 0.5 | 1.9 | 1.0 | 79.3 | 58.4 | 49.1 | 47.6 | 25.0 | 1,615.0 | 30.9 |
| $(5,3)$ | 608.0 | 1,605.0 | 563.2 | 99.7 | 662.8 | 0.9 | 1.1 | 0.2 | 24.7 | 3.7 | - | - | - | 1,605.0 | 55.0 |
| $(8006,4)$ |  | 612.0 |  |  |  |  |  |  |  |  |  |  |  | 612.0 |  |
| ( 4,6) | 229.6 | 606.0 | 212.6 | 16.8 | 229.5 | 0.9 | 1.0 | 0.1 | 36.1 | 15.1 | 13.5 | 13.5 | 1.0 | 606.0 | 60.0 |
| $(6,2)$ | 218.2 | 576.0 | 202.1 | 9.1 | 211.2 | 1.0 | 1.0 | 0.0 | 21.9 | 1.0 | - | - | - | 576.0 | 62.0 |
| $(8002,7)$ |  | 72.0 |  |  |  |  |  |  |  |  |  |  |  | 72.0 |  |
| $(7,5)$ | 3.1 | 11.0 | 4.2 | 3.7 | 7.8 | 0.5 | 2.5 | 1.2 | 1,241.6 | 1,226.7 | 1,220.8 | 1,220.3 | 100.0 | 11.0 | 23.9 |
| $(5,7)$ | 4.2 | 15.0 | 5.6 | 0.6 | 6.3 | 0.9 | 1.5 | 0.2 | 25.1 | 2.5 | 0.1 | - | - | 15.0 | 40.5 |
| ( 5,6) | 0.1 | 5.0 | 0.1 | 0.1 | 0.2 | 0.4 | 3.2 | 1.8 | 1,123.1 | 1,122.7 | 1,122.5 | 1,122.4 | 40.0 | 5.0 | 18.9 |
| $(6,5)$ | 0.0 | 4.0 | 0.1 | 1.5 | 1.5 | 0.0 | 40.0 | 38.7 | 1,102.0 | 1,101.5 | 1,100.8 | 1,099.5 | 100.0 | 4.0 | 1.5 |
| $(6,8)$ | 8.9 | 33.0 | 11.9 | 1.5 | 13.4 | 0.9 | 1.5 | 0.2 | 24.3 | 2.6 | - | - | - | 33.0 | 40.1 |
| $(8,6)$ | 1.4 | 5.0 | 1.8 | 0.7 | 2.6 | 0.7 | 1.9 | 0.6 | 1,892.8 | 1,881.6 | 1,876.2 | 1,875.8 | 100.0 | 5.0 | 31.9 |
| $(8004,8)$ |  | 79.0 |  |  |  |  |  |  |  |  |  |  |  | 79.0 |  |


| CASE 3 | VEHICLE |  | VEHICLE MINUTES |  |  | $\begin{aligned} & \hline \text { RATIO } \\ & \hline \text { MOVE/ } \\ & \text { TOTAL } \\ & \hline \end{aligned}$ | MINUTES/MILE |  | SECONDS/VEHICLE |  |  | AVERAGE VALUES |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\begin{array}{\|c} \hline \text { MOVE } \\ \text { TIME } \end{array}$ | $\begin{aligned} & \hline \text { DELAY } \\ & \text { TIME } \end{aligned}$ | $\begin{gathered} \hline \text { TOTAL } \\ \text { TIME } \\ \hline \end{gathered}$ |  | $\begin{gathered} \hline \text { TOTAL } \\ \text { TIME } \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { DELAY } \\ \text { TIME } \\ \hline \end{gathered}$ | $\begin{aligned} & \hline \text { TOTAL } \\ & \text { TIME } \\ & \hline \end{aligned}$ | $\begin{gathered} \hline \text { DELAY } \\ \text { TIME } \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { QUEUE* } \\ \text { TIME } \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { STOP* } \\ \text { TIME } \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { STOPS } \\ (\%) \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { VOLUME } \\ \text { VPH } \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { SPEED } \\ \text { MPH } \end{gathered}$ |
| LINK | MILES | TRIPS |  |  |  |  |  |  |  |  |  |  |  |  |  |
| (8001,1) |  | 1,681.0 |  |  |  |  |  |  |  |  |  |  |  | 1,681.0 |  |
| $(1,3)$ | 793.1 | 1,675.0 | 734.6 | 37.9 | 772.5 | 1.0 | 1.0 | 0.1 | 27.6 | 1.4 | - | - | - | 1,675.0 | 61.6 |
| $(3,5)$ | 502.8 | 1,770.0 | 465.8 | 68.0 | 533.8 | 0.9 | 1.1 | 0.1 | 18.1 | 2.3 | 0.1 | - | - | 1,770.0 | 56.5 |
| $(5,7)$ | 507.7 | 1,787.0 | 470.3 | 67.9 | 538.2 | 0.9 | 1.1 | 0.1 | 18.0 | 2.3 | - | - | - | 1,787.0 | 56.6 |
| $(7,9)$ | 818.2 | 1,728.0 | 757.9 | 79.5 | 837.4 | 0.9 | 1.0 | 0.1 | 29.0 | 2.8 | - | - | - | 1,728.0 | 58.6 |
| $(8004,10)$ |  | 612.0 |  |  |  |  |  |  |  |  |  |  |  | 612.0 |  |
| $(10,8)$ | 289.3 | 611.0 | 268.0 | 10.5 | 278.5 | 1.0 | 1.0 | 0.0 | 27.3 | 1.1 | - | - | - | 611.0 | 62.3 |
| $(8,6)$ | 188.9 | 665.0 | 175.0 | 26.0 | 201.0 | 0.9 | 1.1 | 0.1 | 18.1 | 2.4 | 0.2 | 0.2 | 2.0 | 665.0 | 56.4 |
| $(6,4)$ | 196.0 | 690.0 | 181.6 | 34.6 | 216.2 | 0.8 | 1.1 | 0.2 | 18.8 | 3.0 | 0.1 | - | - | 690.0 | 54.4 |
| $(4,2)$ | 279.8 | 591.0 | 259.2 | 13.0 | 272.2 | 1.0 | 1.0 | 0.1 | 27.5 | 1.3 | - | - | - | 591.0 | 61.7 |
| $(4,3)$ | 1.1 | 97.0 | 2.2 | 22.5 | 24.7 | 0.1 | 22.4 | 20.4 | 15.3 | 13.9 | 14.1 | 13.9 | 63.0 | 97.0 | 2.7 |
| $(7,8)$ | 0.7 | 57.0 | 1.3 | 1.8 | 3.1 | 0.4 | 4.8 | 2.8 | 3.3 | 1.9 | 2.3 | 2.2 | 45.0 | 57.0 | 12.5 |
| $(8005,11)$ |  | 118.0 |  |  |  |  |  |  |  |  |  |  |  | 118.0 |  |
| $(11,6)$ | 43.0 | 117.0 | 57.3 | 17.1 | 74.4 | 0.8 | 1.7 | 0.4 | 37.8 | 8.7 | 3.8 | 3.7 | 100.0 | 117.0 | 34.7 |
| $(6,11)$ | 33.4 | 91.0 | 44.6 | 4.8 | 49.4 | 0.9 | 1.5 | 0.1 | 32.3 | 3.2 | - | - | - | 91.0 | 40.6 |
| $(6,5)$ | 0.1 | 11.0 | 0.2 | 7.3 | 7.5 | 0.0 | 60.0 | 58.7 | 39.2 | 38.3 | 38.8 | 37.8 | 72.0 | 11.0 | 1.0 |
| ( 5,6) | 0.1 | 8.0 | 0.1 | 3.3 | 3.4 | 0.0 | 37.2 | 35.9 | 25.4 | 24.5 | 23.1 | 21.1 | 50.0 | 8.0 | 1.6 |
| $(5,12)$ | 18.9 | 50.0 | 25.3 | 3.0 | 28.3 | 0.9 | 1.5 | 0.2 | 33.8 | 3.6 | 0.1 | - | - | 50.0 | 40.2 |
| $(12,5)$ | 26.9 | 71.0 | 35.9 | 17.6 | 53.4 | 0.7 | 2.0 | 0.7 | 44.3 | 14.5 | 10.0 | 9.9 | 100.0 | 71.0 | 30.2 |
| $(8006,12)$ |  | 72.0 |  |  |  |  |  |  |  |  |  |  |  | 72.0 |  |

Table 4.2a: Site 1 Queue Measures

| EXISTING VEH MINUTE |  |  | $\begin{array}{r} \hline \text { AVERAGE } \\ \text { OCCUPANC } \\ \text { (VEHICLE } \end{array}$ | CONGESTION |  | QUEUE LENGTH |  |  |  |  |  |  |  |  |  |  |  |  |  | NUMBE OF LAN CHANGE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | QUEU电 STOP  <br> TIME TIME |  |  |  |  | AVERAGE QUEUE BY LANE |  |  |  |  |  |  | MAXIMUM QUEUE BY LAN |  |  |  |  |  |  |  |
| LINK |  |  | (\%) | FAILURE | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |  |
| $(1,5)$ | 78.8 | 78.6 |  | 4.4 | 2.1 | - | - | - | - | - | - | - | 1.0 | 1.0 | 2.0 | - | - | - | - | 2.0 | 121.0 |
| $(5,3)$ | 0.1 | 0.1 | 3.0 | 1.5 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 49.0 |
| $(4,6)$ | 2,238.8 | 2,097.2 | 59.4 | 28.3 | - | 4.0 | 33.0 | - | - | - | - | 6.0 | 28.0 | 68.0 | - | - | - | - | 9.0 | 756.0 |
| $(6,2)$ | - | - | 12.9 | 6.5 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 848.0 |
| $(7,5)$ | 2,199.9 | 2,199.1 | 37.7 | 50.2 | - | 37.0 | - | - | - | - | - | - | 81.0 | - | - | - | - | - | - | - |
| $(5,7)$ | 0.1 | 0.1 | 0.4 | 0.5 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| $(5,6)$ | 139.6 | 139.4 | 3.0 | 118.8 | - | 2.0 | - | - | - | - | - | - | 3.0 | - | - | - | - | - | - | - |
| $(6,5)$ | 97.0 | 96.5 | 1.7 | 67.2 | - | 2.0 | - | - | - | - | - | - | 2.0 | - | - | - | - | - | - | - |
| $(6,8)$ | - | - | 0.5 | 0.7 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| $(8,6)$ | 2,100.4 | 2,098.8 | 36.1 | 50.2 | - | 35.0 | - | - | - | - | - | - | 75.0 | - | - | - | - | - | - | - |


| CASE 3 | VEH MINUTE |  | $\begin{array}{\|c\|} \hline \text { AVERAGE } \\ \text { OCCUPANO } \\ \text { (VEHICLE } \\ \hline \end{array}$ | CONGESTION |  | QUEUE LENGTH |  |  |  |  |  |  |  |  |  |  |  |  |  | NUMBE OF LAN |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | QUEU电 STOP <br> TIME TIME |  |  |  |  |  | AVER | AG | QU | UE | BY | ANE |  | MAX | MU | Q | U | BY | AN, |  |
| LINK |  |  | (\%) | FAILUR | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |  |  |
| $(1,3)$ | 0.1 | 0.1 |  | 3.7 | 1.5 | - | - | - | - | - | - | - | - | 1.0 | - | - | - | - | - | - | 8.0 |
| $(3,5)$ | 6.7 | 6.1 | 3.3 | 2.2 | - | - | - | - | - | - | - | - | 2.0 | 2.0 | - | - | - | - | - | 102.0 |
| $(5,7)$ | 0.5 | - | 2.7 | 1.4 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 67.0 |
| $(7,9)$ | - | - | 3.5 | 1.4 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 42.0 |
| $(10,8)$ | - | - | 15.3 | 6.1 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 367.0 |
| $(8,6)$ | 8.1 | 6.9 | 10.6 | 7.0 | - | - | - | - | - | - | - | - | 3.0 | 6.0 | - | - | - | - | - | 374.0 |
| $(6,4)$ | 1.7 | 1.3 | 11.1 | 5.9 | - | - | - | - | - | - | - | - | 4.0 | 2.0 | - | - | - | - | - | 409.0 |
| $(4,2)$ | - | - | 16.4 | 6.6 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 552.0 |
| $(4,3)$ | 2.0 | 1.9 | 0.1 | 4.0 | - | - | - | - | - | - | - | - | 2.0 | - | - | - | - | - | - | - |
| $(7,8)$ | 22.5 | 22.4 | 0.6 | 20.3 | - | - | - | - | - | - | - | - | 3.0 | - | - | - | - | - | - | - |
| $(11,6)$ | 23.1 | 22.6 | 2.1 | 2.2 | - | - | - | - | - | - | - | - | 3.0 | - | - | - | - | - | - | - |
| $(6,11)$ | 0.1 | - | 1.1 | 1.1 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| $(6,5)$ | 7.5 | 6.7 | 0.3 | 9.3 | - | - | - | - | - | - | - | - | 1.0 | - | - | - | - | - | - | - |
| $(5,6)$ | 29.0 | 28.0 | 0.8 | 27.0 | - | - | - | - | - | - | - | - | 2.0 | - | - | - | - | - | - | - |
| $(5,12)$ | 0.3 | 0.1 | 1.9 | 1.9 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| $(12,5)$ | 6.8 | 6.5 | 1.8 | 1.8 | - | - | - | - | - | - | - | - | 2.0 | - | - | - | - | - | - | - |

Table 4.2b: Site 2 Queue Measures

| EXISTING | VEH MINUTE |  |  | CONGESTION |  | QUEUE LENGTH |  |  |  |  |  |  |  |  |  |  |  |  |  | NUMBEI OF LANH CHANGE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} \hline \text { QUEU申 } \\ \text { TIME } \\ \hline \end{gathered}$ | $\begin{aligned} & \hline \text { STOP } \\ & \text { TIME } \\ & \hline \end{aligned}$ |  | STORAGE PHASE |  | AVERAGE QUEUE BY LANE |  |  |  |  |  |  | MAXIMUM QUEUE BY LANE |  |  |  |  |  |  |  |
| LINK |  |  |  | (\%) | FAILUR | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 1 | 2 | 3 | 4 | 5 | 6 | 7 |  |
| $(1,5)$ | 1,383.1 | 1,340.5 | 37.4 | 15.0 | - | 1.0 | 10.0 | - | - | - | - | 14.0 | 9.0 | 31.0 | - | 0 | - | - | 31.0 | 680.0 |
| $(5,3)$ | - | - | 11.6 | 5.8 | - | - | - | - | - | - | - | - | - | - | - | 0 | - | - | - | 734.0 |
| $(4,6)$ | 139.1 | 138.8 | 6.7 | 2.7 | - | - | - | - | - | - | - | 2.0 | 1.0 | 3.0 | - | 0 | - | - | 5.0 | 53.0 |
| $(6,2)$ | - | - | 4.0 | 2.0 | - | - | - | - | - | - | - | - | - | - | - | 0 | - | - | - | 77.0 |
| $(7,5)$ | 1,485.3 | 1,484.7 | 25.7 | 34.3 | - | 25.0 | - | - | - | - | - | - | 61.0 | - | - | 0 | - | - | - | - |
| $(5,7)$ | - | - | 0.2 | 0.3 | - | - | - | - | - | - | - | - | - | - | - | 0 | - | - | - | - |
| $(5,6)$ | 149.7 | 149.6 | 3.3 | 130.8 | - | 2.0 | - | - | - | - | - | - | 3.0 | - | - | 0 | - | - | - | - |
| $(6,5)$ | 110.1 | 109.9 | 1.9 | 76.0 | - | 2.0 | - | - | - | - | - | - | 2.0 | - | - | 0 | - | - | - | - |
| $(6,8)$ | - | - | 0.4 | 0.5 | - | - | - | - | - | - | - | - | - | - | - | 0 | - | - | - | - |
| $(8,6)$ | 2,501.6 | 2,501.0 | 42.7 | 59.3 | - | 42.0 | - | - | - | - | - | - | 75.0 | - | - | 0 | - | - | - | - |


| CASE 3 | VEH MINUTE |  | AVERAGEOCCUPANO(VEHICLE | CONGESTION |  | QUEUE LENGTH |  |  |  |  |  |  |  |  |  |  |  |  |  | $\begin{array}{\|l\|} \hline \text { NUMBE } \\ \text { OF LANE } \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | QUEU¢ | STOP |  |  |  | AVERAGE QUEUE BY LANE |  |  |  |  |  |  | MAXIMUM QUEUE BY LAN |  |  |  |  |  |  |  |
| LINK | TIME | TIME |  | (\%) | FAILUR | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | CHANGE |
| $(1,3)$ | 0.2 | 0.2 | 13.2 | 5.3 | - | - | - | - | - | - | - | - | 1.0 | - | - | 0 | - | - | - | 303.0 |
| $(3,5)$ | 1.8 | 1.4 | 9.4 | 6.3 | - | - | - | - | - | - | - | - | 2.0 | 5.0 | - | 0 | - | - | - | 321.0 |
| $(5,7)$ | 0.3 | - | 9.4 | 5.0 | - | - | - | - | - | - | - | - | - | - | - | 0 | - | - | - | 369.0 |
| $(7,9)$ | - | - | 14.5 | 5.8 | - | - | - | - | - | - | - | - | - | - | - | 0 | - | - | - | 524.0 |
| $(10,8)$ | - | - | 5.1 | 2.0 | - | - | - | - | - | - | - | - | 1.0 | - | - | 0 | - | - | - | 11.0 |
| $(8,6)$ | 2.5 | 2.3 | 3.9 | 2.6 | - | - | - | - | - | - | - | - | 1.0 | 2.0 | - | 0 | - | - | - | 89.0 |
| $(6,4)$ | 1.2 | 0.2 | 4.1 | 2.2 | - | - | - | - | - | - | - | - | - | - | - | 0 | - | - | 1.0 | 110.0 |
| (4,2) | - | - | 5.0 | 2.0 | - | - | - | - | - | - | - | - | - | - | - | 0 | - | - | - | 107.0 |
| $(4,3)$ | 22.9 | 22.4 | 0.6 | 21.0 | - | - | - | - | - | - | - | - | 3.0 | - | - | 0 | - | - | - | - |
| $(7,8)$ | 2.2 | 2.1 | 0.1 | 3.7 | - | - | - | - | - | - | - | - | 2.0 | - | - | 0 | - | - | - | - |
| $(11,6)$ | 7.5 | 7.3 | 1.8 | 1.9 | - | - | - | - | - | - | - | - | 1.0 | - | - | 0 | - | - | - | - |
| (6,11) | 0.1 | - | 1.3 | 1.3 | - | - | - | - | - | - | - | - | - | - | - | 0 | - | - | - | - |
| $(6,5)$ | 7.8 | 7.6 | 0.2 | 8.0 | - | - | - | - | - | - | - | - | 2.0 | - | - | 0 | - | - | - | - |
| $(5,6)$ | 3.1 | 2.8 | 0.1 | 3.7 | - | - | - | - | - | - | - | - | 1.0 | - | - | 0 | - | - | - | - |
| $(5,12)$ | 0.1 | - | 0.7 | 0.7 | - | - | - | - | - | - | - | - | - | - | - | 0 | - | - | - | - |
| $(12,5)$ | 12.2 | 12.1 | 1.6 | 1.6 | - | - | - | - | - | - | - | - | 2.0 | - | - | 0 | - | - | - | - |

Table 4.3a: Site 1 Fuel Consumption Measures

| EXISTING | FUEL CONSUMPTION |  |  |  |  |  |  |  |  |  |  |
| :---: | ---: | ---: | ---: | ---: | ---: | ---: | :---: | :---: | :---: | :---: | :---: |
|  | Gallons |  |  |  |  |  |  |  | MPG |  |  |
| LINK | Avg. Auto | Aggressive Auto | Truck | Avg. Auto | Aggressive Auto | Truck |  |  |  |  |  |
| $(5,3)$ | 2.69 | 4.22 | 6.6 | 14.82 | 22.38 | 2.58 |  |  |  |  |  |
| $(6,8)$ | 0.21 | 0.47 | 0.59 | 9.96 | 17.92 | 1.8 |  |  |  |  |  |
| $(6,2)$ | 13.59 | 24.81 | 35.41 | 10.72 | 18.49 | 2.36 |  |  |  |  |  |
| $(5,7)$ | 0.16 | 0.34 | 1.08 | 10.33 | 16.2 | 1.9 |  |  |  |  |  |
| $(6,5)$ | 0.01 | 0.4 | 0.78 | 5.85 | 0.49 | 0.02 |  |  |  |  |  |
| $(4,6)$ | 18.4 | 41.4 | 34.68 | 8.06 | 11.43 | 2.47 |  |  |  |  |  |
| $(8,6)$ | 3.11 | 14.05 | 1.18 | 1.23 | 0.95 | 0.46 |  |  |  |  |  |
| $(5,6)$ | 0.37 | 0.7 | 0 | 0.02 | 0.03 | 0 |  |  |  |  |  |
| $(1,5)$ | 3.05 | 5.09 | 7.35 | 12.63 | 17.86 | 2.43 |  |  |  |  |  |
| $(7,5)$ | 7.11 | 10.75 | 0.37 | 0.78 | 0.86 | 0.26 |  |  |  |  |  |


| CASE 3 | FUEL CONSUMPTION |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | :---: | :---: | :---: |
|  | Gallons |  |  |  |  |  |  | MPG |  |
| LINK | Avg. Auto | Aggressive Auto | Truck | Avg. Auto | Aggressive Auto | Truck |  |  |  |
| $(7,9)$ | 2.47 | 4.57 | 8.15 | 19.43 | 26.8 | 2.71 |  |  |  |
| $(5,12)$ | 1.29 | 1.94 | 1.95 | 11.28 | 19.57 | 2.15 |  |  |  |
| $(4,2)$ | 11.71 | 24.04 | 33.05 | 17.13 | 25.27 | 3.17 |  |  |  |
| $(6,11)$ | 0.43 | 1.09 | 0.98 | 11.89 | 20.01 | 2.53 |  |  |  |
| $(6,4)$ | 9.04 | 17.05 | 21.8 | 13.9 | 22.48 | 3.03 |  |  |  |
| $(5,6)$ | 0.04 | 0.21 | 0.01 | 0.83 | 0.8 | 0.13 |  |  |  |
| $(5,7)$ | 2.64 | 4.16 | 5.5 | 11.88 | 19.05 | 2.58 |  |  |  |
| $(3,5)$ | 2.69 | 4.8 | 6.13 | 13.34 | 19.01 | 2.79 |  |  |  |
| $(6,5)$ | 0.02 | 0.06 | 0.01 | 3.98 | 1.6 | 0.77 |  |  |  |
| $(8,6)$ | 6.49 | 13.87 | 17.74 | 18.3 | 26.92 | 3.81 |  |  |  |
| $(4,3)$ | 0.01 | 0.03 | 0.02 | 9.18 | 13.01 | 3.1 |  |  |  |
| $(7,8)$ | 0.05 | 0.13 | 0.01 | 0.95 | 0.79 | 1.8 |  |  |  |
| $(12,5)$ | 0.48 | 1.12 | 0.19 | 16.33 | 25.14 | 3.97 |  |  |  |
| $(11,6)$ | 0.93 | 1.27 | 0.37 | 15.27 | 23.09 | 2.96 |  |  |  |
| $(10,8)$ | 11.58 | 24.04 | 39.98 | 16.33 | 25.08 | 2.71 |  |  |  |
| $(1,3)$ | 3.15 | 4.93 | 9.27 | 15.4 | 23.19 | 2.41 |  |  |  |

Table 4.3b: Site 2 Fuel Consumption Measures

| EXISTING | FUEL CONSUMPTION |  |  |  |  |  |  |
| :---: | ---: | ---: | ---: | ---: | ---: | ---: | :---: |
|  | Gallons |  |  |  | MPG |  |  |
| LINK | Avg. Auto | Aggressive Auto | Truck | Avg. Auto | Aggressive Auto | Truck |  |
| $(5,3)$ | 13.84 | 23.96 | 27.17 | 9.96 | 17.08 | 2.28 |  |
| $(6,8)$ | 0.23 | 0.38 | 0.57 | 8.19 | 14.97 | 1.85 |  |
| $(6,2)$ | 2.37 | 5.64 | 9.33 | 19.5 | 26.05 | 2.68 |  |
| $(5,7)$ | 0.06 | 0.18 | 0.29 | 9.92 | 17.16 | 1.93 |  |
| $(6,5)$ | 0.01 | 0.44 | 0.86 | 0.47 | 0.04 | 0 |  |
| $(4,6)$ | 3.68 | 7.43 | 12.14 | 12.98 | 20.51 | 2.23 |  |
| $(8,6)$ | 4.24 | 15.36 | 1.36 | 0.66 | 0.54 | 0.25 |  |
| $(5,6)$ | 0 | 1.16 | 0 | 10.49 | 0.02 | 0 |  |
| $(1,5)$ | 12.59 | 28.44 | 25.18 | 10.99 | 14.69 | 2.47 |  |
| $(7,5)$ | 4.85 | 7.44 | 0.44 | 0.96 | 1.17 | 1.14 |  |


| CASE 3 | FUEL CONSUMPTION |  |  |  |  |  |
| :---: | ---: | ---: | ---: | ---: | ---: | ---: |
|  | Gallons |  |  |  |  |  |
| LINK | Avg. Auto | Aggressive Auto | Truck | Avg. Auto | Aggressive Auto | Truck |
| $(7,9)$ | 10.73 | 21.64 | 26.53 | 17.32 | 25.61 | 3.01 |
| $(5,12)$ | 0.32 | 0.62 | 0.82 | 11.83 | 20.93 | 2.67 |
| $(4,2)$ | 3.22 | 7.06 | 10.76 | 18.96 | 27.01 | 2.69 |
| $(6,11)$ | 0.72 | 1.04 | 1.67 | 11.99 | 19.76 | 2.17 |
| $(6,4)$ | 3.44 | 6.24 | 6.87 | 12.17 | 21.21 | 2.88 |
| $(5,6)$ | 0 | 0.03 | 0 | 0.32 | 2.02 | 0 |
| $(5,7)$ | 7.22 | 14.38 | 15.29 | 15.74 | 23.98 | 3.19 |
| $(3,5)$ | 6.81 | 13.75 | 14.43 | 16.45 | 24.81 | 3.49 |
| $(6,5)$ | 0.01 | 0.05 | 0 | 1.07 | 0.48 | 0 |
| $(8,6)$ | 2.24 | 5.29 | 7.49 | 17.69 | 24.15 | 3.02 |
| $(4,3)$ | 0.03 | 0.17 | 0.03 | 3.8 | 1.83 | 1.32 |
| $(7,8)$ | 0.01 | 0.02 | 0 | 10.95 | 8.49 | 5.86 |
| $(12,5)$ | 0.27 | 0.83 | 0.19 | 20.47 | 24.72 | 4.01 |
| $(11,6)$ | 0.79 | 1.03 | 0.16 | 17.35 | 27.34 | 4.67 |
| $(10,8)$ | 3.82 | 8.01 | 15.94 | 15.68 | 23.67 | 2.24 |
| $(1,3)$ | 10.76 | 21.73 | 31.15 | 16.04 | 24.4 | 2.53 |

Table 4.4a: Site 1 Emissions Measures

| EXISTING | EMISSIONS OF HC (GRAMS/MILE) |  |  | EMISSIONS OF CO (GRAMS/MILE) |  | EMISSIONS OF NO (GRAMS/MILE) |  |  |  |  |
| :---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| LINK | Avg. Auto | Aggressive Auto | Truck | Avg. Auto | Aggressive Auto | Truck | Avg. Auto | Aggressive Auto | Truck |  |
| $(5,3)$ | 0.2 | 0.2 | 14.9 | 11.9 | 12.4 | 288.9 | 1.0 | 34.9 |  |  |
| $(6,8)$ | 0.3 | 0.3 | 19.1 | 25.2 | 26.3 | 341.2 | 1.2 | 1.0 | 3.0 | 49.9 |
| $(6,2)$ | 0.3 | 0.3 | 15.5 | 25.6 | 25.0 | 292.1 | 1.3 | 1.1 | 38.1 |  |
| $(5,7)$ | 0.3 | 0.4 | 18.0 | 20.0 | 30.2 | 321.7 | 1.1 | 46.8 |  |  |
| $(6,5)$ | 0.2 | 0.1 | $1,228.8$ | 6.3 | 34.2 | $* * * * * * *$ | 1.0 | 1.1 | 46.8 |  |
| $(4,6)$ | 0.3 | 0.3 | 14.4 | 21.2 | 25.0 | 263.3 | 1.3 | 0.3 | 733.1 |  |
| $(8,6)$ | 0.4 | 0.5 | 59.3 | 44.3 | 55.3 | 783.6 | 1.7 | 1.2 | 31.1 |  |
| $(5,6)$ | 0.7 | 0.1 | - | $1,089.4$ | 467.5 | - | 3.7 | 1.4 | 66.0 |  |
| $(1,5)$ | 0.3 | 0.3 | 16.6 | 19.4 | 21.9 | 333.2 | 1.1 | 0.4 | - |  |
| $(7,5)$ | 0.4 | 0.5 | 101.7 | 51.4 | 55.7 | $1,259.9$ | 1.6 | 1.1 | 36.9 |  |


| CASE 3 | EMISSIONS OF HC (GRAMS/MILE) |  |  |  |  |  |  |  |  |
| :---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| EMISSIONS OF CO (GRAMS/MILE) |  | EMISSIONS OF NO (GRAMS/MILE) |  |  |  |  |  |  |  |
| LINK | Avg. Auto | Aggressive Auto | Truck | Avg. Auto | Aggressive Auto | Truck | Avg. Auto | Aggressive Auto | Truck |
| $(7,9)$ | 0.1 | 0.1 | 14.0 | 4.7 | 4.4 | 270.9 | 0.8 | 0.8 | 33.1 |
| $(5,12)$ | 0.2 | 0.3 | 15.9 | 19.8 | 21.3 | 283.3 | 1.0 | 0.8 | 41.3 |
| $(4,2)$ | 0.2 | 0.2 | 11.7 | 10.2 | 11.0 | 220.7 | 0.8 | 0.7 | 27.8 |
| $(6,11)$ | 0.2 | 0.2 | 13.4 | 17.6 | 20.4 | 236.7 | 0.9 | 0.8 | 34.8 |
| $(6,4)$ | 0.2 | 0.2 | 12.1 | 15.9 | 15.9 | 228.0 | 1.0 | 0.8 | 29.2 |
| $(5,6)$ | 0.4 | 0.4 | 197.1 | 33.5 | 36.0 | $2,283.6$ | 2.2 | 1.9 | 112.6 |
| $(5,7)$ | 0.3 | 0.3 | 14.6 | 20.2 | 21.6 | 281.3 | 1.2 | 1.1 | 34.7 |
| $(3,5)$ | 0.2 | 0.3 | 13.1 | 15.7 | 22.4 | 247.2 | 1.1 | 1.1 | 31.9 |
| $(6,5)$ | 0.2 | 0.1 | 33.8 | 7.9 | 13.4 | 400.3 | 1.1 | 0.5 | 24.9 |
| $(8,6)$ | 0.1 | 0.1 | 9.4 | 8.9 | 9.1 | 172.8 | 0.7 | 0.6 | 22.8 |
| $(4,3)$ | 0.1 | 0.0 | 8.5 | 3.8 | 3.0 | 110.4 | 0.5 | 0.1 | 11.2 |
| $(7,8)$ | 0.1 | 0.1 | 14.7 | 19.1 | 21.8 | 186.9 | 0.2 | 0.3 | 17.7 |
| $(12,5)$ | 0.2 | 0.2 | 8.6 | 12.5 | 13.7 | 150.9 | 0.6 | 0.5 | 20.9 |
| $(11,6)$ | 0.2 | 0.2 | 11.5 | 13.1 | 14.4 | 204.0 | 0.6 | 0.5 | 28.2 |
| $(10,8)$ | 0.2 | 0.2 | 14.7 | 12.2 | 13.1 | 293.0 | 0.8 | 0.8 | 32.9 |
| $(1,3)$ | 0.2 | 0.2 | 16.7 | 11.7 | 13.0 | 336.2 | 0.9 | 0.9 | 37.3 |

Table 4.4b: Site 2 Emissions Measures

| EXISTING | EMISSIONS OF HC (GRAMS/MILE) |  |  | EMISSIONS OF CO (GRAMS/MILE) |  |  | EMISSIONS OF NO (GRAMS/MILE) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LINK | Avg. Auto | Aggressive Auto | Truck | Avg. Auto | Aggressive Auto | Truck | Avg. Auto | Aggressive Auto | Truck |
| $(5,3)$ | 0.4 | 0.4 | 16.1 | 28.4 | 29.0 | 301.9 | 1.4 | 1.3 | 39.5 |
| $(6,8)$ | 0.4 | 0.4 | 18.7 | 32.5 | 35.8 | 333.5 | 1.6 | 1.3 | 48.3 |
| $(6,2)$ | 0.1 | 0.1 | 14.3 | 4.8 | 6.4 | 277.7 | 0.8 | 0.8 | 33.6 |
| $(5,7)$ | 0.3 | 0.3 | 17.8 | 23.8 | 28.4 | 316.4 | 1.2 | 1.0 | 46.0 |
| $(6,5)$ | - | 0.1 | 6,207.3 | 36.2 | 362.3 | ******* | - | 0.5 | 3,547.1 |
| $(4,6)$ | 0.2 | 0.2 | 18.4 | 15.1 | 16.1 | 376.6 | 1.0 | 0.9 | 39.9 |
| $(8,6)$ | 0.4 | 0.5 | 105.2 | 53.9 | 72.3 | 1,316.0 | 1.6 | 1.5 | 94.2 |
| $(5,6)$ | - | - | - | 1.9 | 692.8 | - | - | - | - |
| $(1,5)$ | 0.2 | 0.3 | 15.6 | 16.6 | 20.1 | 305.0 | 1.0 | 0.9 | 33.7 |
| $(7,5)$ | 0.4 | 0.4 | 25.3 | 49.0 | 47.9 | 360.5 | 1.6 | 1.2 | 38.0 |


| CASE 3 | EMISSIONS OF HC (GRAMS/MILE) |  |  | EMISSIONS OF CO (GRAMS/MILE) |  |  | EMISSIONS OF NO (GRAMS/MILE) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LINK | Avg. Auto | Aggressive Auto | Truck | Avg. Auto | Aggressive Auto | Truck | Avg. Auto | Aggressive Auto | Truck |
| $(7,9)$ | 0.1 | 0.2 | 12.6 | 9.5 | 10.4 | 242.3 | 0.8 | 0.7 | 29.4 |
| $(5,12)$ | 0.2 | 0.2 | 12.7 | 19.0 | 18.6 | 224.2 | 1.0 | 0.7 | 33.0 |
| $(4,2)$ | 0.1 | 0.1 | 14.5 | 6.0 | 5.6 | 285.7 | 0.8 | 0.7 | 33.3 |
| $(6,11)$ | 0.2 | 0.3 | 15.8 | 18.8 | 21.4 | 279.4 | 1.0 | 0.8 | 40.8 |
| $(6,4)$ | 0.3 | 0.2 | 13.2 | 19.4 | 17.2 | 254.6 | 1.2 | 1.0 | 31.0 |
| $(5,6)$ | - | 0.1 | - | 51.0 | 11.6 | - | - | 0.6 | - |
| $(5,7)$ | 0.2 | 0.2 | 11.6 | 12.4 | 13.1 | 219.9 | 0.8 | 0.8 | 27.7 |
| $(3,5)$ | 0.2 | 0.2 | 10.5 | 11.0 | 11.6 | 196.1 | 0.8 | 0.7 | 25.2 |
| $(6,5)$ | 0.3 | 0.4 | - | 24.4 | 51.3 | - | 1.6 | 1.6 | - |
| $(8,6)$ | 0.1 | 0.2 | 12.4 | 7.8 | 10.9 | 235.9 | 0.8 | 0.8 | 29.6 |
| $(4,3)$ | 0.1 | 0.1 | 19.8 | 7.0 | 13.8 | 241.7 | 0.4 | 0.6 | 17.8 |
| $(7,8)$ | 0.0 | 0.0 | 4.5 | 2.1 | 2.6 | 55.1 | 0.1 | 0.0 | 4.4 |
| $(12,5)$ | 0.1 | 0.2 | 8.0 | 7.4 | 12.1 | 135.4 | 0.4 | 0.5 | 19.9 |
| $(11,6)$ | 0.2 | 0.1 | 7.1 | 11.7 | 10.5 | 120.8 | 0.5 | 0.4 | 17.1 |
| $(10,8)$ | 0.2 | 0.2 | 18.3 | 11.5 | 12.4 | 371.2 | 0.9 | 0.9 | 40.2 |
| $(1,3)$ | 0.2 | 0.2 | 16.0 | 12.2 | 13.7 | 322.4 | 0.8 | 0.8 | 35.4 |

Table 4.5a: Link Specific Comparisons of Performance Measures - Site 1

| LINK |  | DELAY PERVEHICLE (SEC) |  | QUEUE |  | FUEL CONSUMPTION(GAL) |  | HC EMISSIONS (GRAMS/MILE) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| EXISTING | CASE 3 | EXISTING | CASE 3 | EXISTING | CASE 3 | EXISTING | CASE 3 | EXISTING | CASE 3 |
| $(4,6)$ | $(8,6)$ | 109.7 | 2.7 | 19 | - | 29.9 | 10.2 | 0.6 | 0.3 |
| $(7,5)$ | $(12,5)$ | 1,409.7 | 9.5 | 19 | - | 9.0 | 0.8 | 0.9 | 0.4 |
| $(5,6)$ | $(5,6)$ | 846.1 | 43.6 | 1 | - | 0.5 | 0.1 | 0.8 | 0.3 |
| $(6,5)$ | $(6,5)$ | 172.8 | 18.9 | 1 | - | 0.2 | 0.0 | 0.3 | 0.1 |
| $(8,6)$ | $(11,6)$ | 1,217.6 | 16.1 | 18 | - | 8.6 | 1.1 | 0.9 | 0.4 |

Table 4.5b: Link Specific Comparisons of Performance Measures - Site 2

| LINK |  | DELAY PER <br> VEHICLE (SEC) |  | QUEUE |  | FUEL CONSUMPTION <br> (GAL) |  | HC EMISSIONS <br> (GRAMS/MILE) |  |
| :---: | :---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| EXISTING | CASE 3 | EXISTING | CASE 3 | EXISTING | CASE 3 | EXISTING | CASE 3 | EXISTING | CASE 3 |
| $(4,6)$ | $(8,6)$ | 15.1 | 2.4 | 13 | - | 5.6 | 3.8 | 0.2 | 0.2 |
| $(7,5)$ | $(12,5)$ | 2.5 | 14.5 | - | - | 6.1 | 0.6 | 0.4 | 0.2 |
| $(5,6)$ | $(5,6)$ | $1,122.7$ | 24.5 | 1 | - | 0.6 | 0.0 | - | 0.1 |
| $(6,5)$ | $(6,5)$ | $1,101.5$ | 38.3 | 1 | - | 0.2 | 0.0 | 0.1 | 0.4 |
| $(8,6)$ | $(11,6)$ | $1,881.6$ | 2.4 | 21 | - | 9.8 | 0.9 | 0.5 | 0.2 |

Table 4.6a: System-wide Comparisons of Performance Measures - Site 1
Table 4.6a: System-wide Comparisons of Performance Measures - Site 1

| MOE |  | EXISTING | CASE 3 |
| :--- | ---: | ---: | ---: |
| Average total delay in vehicle minute | 152.5 | 34.6 | $77 \%$ |
| Average delay per vehicle in seconds | 376.0 | 9.5 | $97 \%$ |
| Average percent stops | 35.6 | 43.5 | $-22 \%$ |
| Average queue length | 5.7 | - | $100 \%$ |
| Average maximum queue length | 13.0 | 1.0 | $92 \%$ |
| Average fuel consumption (gallons) | 8.0 | 11.8 | $-48 \%$ |
| Average fuel consumption (mpg) | 6.5 | 11.2 | $-72 \%$ |
| Total Emissions of HC (grams/mile) | $1,494.4$ | 415.7 | $72 \%$ |
| Total Emissions of CO (grams/mile) | $5,952.1$ | $6,387.4$ | $-7 \%$ |
| Total Emissions of NO (grams $/ \mathrm{mile}$ ) | $1,153.1$ | 568.1 | $51 \%$ |

Table 4.6b: System-wide Comparisons of Performance Measures - Site 2

| MOE | EXISTING | CASE 3 | \% REDUCTION |
| :--- | ---: | ---: | ---: |
| Average total delay in vehicle minute | 75.7 | 25.9 | $66 \%$ |
| Average delay per vehicle in seconds | 541.6 | 7.8 | $99 \%$ |
| Average percent stops | 36.6 | 27.0 | $26 \%$ |
| Average queue length | 4.1 | - | $100 \%$ |
| Average maximum queue length | 9.3 | 0.7 | $92 \%$ |
| Average fuel consumption (gallons) | 7.0 | 11.1 | $-59 \%$ |
| Average fuel consumption (mpg) | 7.0 | 11.7 | $-67 \%$ |
| Total Emissions of HC (grams/mile) | $6,443.7$ | 195.9 | $97 \%$ |
| Total Emissions of CO (grams/mile) | $5,161.2$ | $3,941.3$ | $24 \%$ |
| Total Emissions of NO (grams/mile) | $3,939.7$ | 441.3 | $89 \%$ |

## V. USING THE HCM/HCS TO EVALUATE ALTERNATIVES

The Highway Capacity Software ${ }^{9}$ implements Part A of the Highway Capacity Manual (HCM) ${ }^{3}$ Chapter 10 (Unsignalized Intersections). Part A of the HCM chapter deals with two-way stop-controlled intersections. It provides an analytical approach to estimate average conditions. The results can be adapted to apply, to a limited extent, to Type II Crossovers. However, as described in this chapter, the HCM approach was found to be inferior to the CORSIM approach (described earlier in Chapter 4).

## INTRODUCTION

The HCM method for two-way stop-controlled intersections assumes that:

- vehicles yield to other movements in priority accorded by normal traffic law,
- gaps used by lower priority vehicles are randomly distributed, however the arrival pattern within a particular time interval may be affected by nearby (within $1 / 4 \mathrm{mile}$ ) signals,
- the first waiting vehicle requires a "critical gap" in conflicting traffic to make its movement, and
- additional vehicles behind the first vehicle require additional "follow-up time" to use that same gap.

To illustrate critical gap and follow-up time, see Figure 5-1 below. Vehicle 1 must wait for a critical gap in the conflicting flow. If that gap equals the critical gap plus the follow-up time, then both Vehicle 1 and Vehicle 2 can make their maneuver in the same gap.


Figure 5-1: Critical Gap and Follow-up Time
As mentioned above, it is assumed that vehicles yield to other movements in priority accorded by normal traffic law. The priority is shown in Table 5-1 and Figure 5-2.

TABLE 5-1: Priority of Streams

| Rank | Movement | Subordinate to: |
| :---: | :---: | :---: |
| $\mathrm{r}=1$ | - through traffic on major road <br> - right turning traffic from major road | - |
| $\mathrm{r}=2$ | - left-turning traffic from major road <br> - right turning traffic onto major road from minor | Rank 1 |
| $\mathrm{r}=3$ | - through traffic on minor road <br> - left-turning traffic from minor road (if a T-intersection) | Ranks 1 and 2 |
| $\mathrm{r}=4$ | - left-turning traffic from minor road (if a 4-leg intersection) | Ranks 1, 2, and 3 |



Figure 5-2: Priority of Streams at Crossover

Two-stage Gap Acceptance

To analyze traffic movements at a crossover, a special procedure called two-stage gap acceptance is used. For example, a minor road left-turning vehicle (Movement 7 in Figure 5-2) might first find a gap in major road traffic coming from the left and then wait for a gap in major road traffic coming from the right (also see Figure 5-3).


Figure 5-3: Two-stage Gap Acceptance

Flared Minor-road Approaches

When the minor road approach is flared or channelized so that two vehicles can wait side-by-side at the stop line (e.g., a right-tuning vehicle and a through vehicle), the capacity of this approach is greater than if only one vehicle can wait at the stop line. This is generally the case at a crossover. The magnitude of this increase in capacity depends on the turning movement flow rates and the storage length to feed the "second position." The resulting capacity will be between that of a single lane approach and that of a twolane approach.

## Input requirements

The input requirements consist of geometric data and traffic flow data. Geometric
data include:

- Number and use of lanes - On major road, this may include a left-turn lane (really a deceleration lane with perhaps some storage space) plus two through lane plus a right-turn lane or a left-turn lane (really a deceleration lane with perhaps some storage space) plus one through lane plus a shared through/right-turn lane;
- Channelization - all locations where right turns are channelized should be noted;
- Raised or striped median storage - Crossovers by their nature have median storage. When using the HCS, this storage space is indicated by selecting "raised median. Generally about 30 ft . is needed to store a passenger car;
- approach grade - downgrades increase capacity while upgrades decrease capacity; and
- flared approaches on minor roads.

Traffic data include:

- vehicular volumes by movement during the peak hour must be indicated. Note that the "peak hour" is the consecutive 60 minute period with the highest volumes. However, is the minor road traffic peaks at a different time than the major road traffic, one should consider any time period that might be congested;
- PHF - The 15 minute flows during the peak hour should be examined to determine one peak hour factor for the crossover traffic. PHF = peak hour volume/(4x Peak 15-minute volume);
- traffic composition - the \% heavy vehicles (i.e., trucks and buses) for each traffic movement should be entered;
- upstream signal data - needed if a signal on the major road is within 0.25 miles of the crossover. Required information includes cycle length, green time for major road traffic, progression speed, arrival type, saturation flow rate, and progressed flow; and
- pedestrian volumes - generally equal to zero for rural crossovers.


## performance measures

The performance measures output by the HCS include delay and level of service. The results can be manually manipulated to also produce average queue length and $95^{\text {th }}$ percentile queue length.

## Delay and Level of Service

The HCS estimates average control delay. Note also that this delay can be directly measured in the field. The LOS criteria are given in the HCM are shown in Table 5-2.

TABLE 5-2: LEVEL-OF-SERVICE CRITERIA

| LOS | AVERAGE CONTROL DELAY, D (sec/veh) |
| :---: | :---: |
| A | $\mathrm{D} \leq 10$ |
| B | $10<\mathrm{D} \leq 15$ |
| C | $15<\mathrm{D} \leq 25$ |
| D | $25<\mathrm{D} \leq 35$ |
| E | $35<\mathrm{D} \leq 50$ |
| F | $50<\mathrm{D}$ |

Note that we can calculate control delay, and therefore level of service, for:

- a single yielding movement
- a minor road approach
- average intersection total delay


## Average Queue Length and Maximum ( $95^{\text {th }}$ percentile) Queue Length

Average Queue Length must be calculated manually. The average queue length will be equal to the average delay per vehicle times the flow rate of the movement (both available from the HCS output). To visualize the units, think of average delay in hours times vehicles per hour ( $\mathrm{hr} \mathrm{x} \mathrm{veh} / \mathrm{hr}=\mathrm{veh}-\mathrm{hr} / \mathrm{hr}=$ veh $=$ vehicles $).$

The expected maximum queue length (also called the $95^{\text {th }}$ percentile queue length or the queue length that will not be exceeded except for $5 \%$ of the time) is found through a nomograph in the HCM. One must manually enter the volume/capacity ratio and the hourly approach volume (available from the HCS output) to find the expected maximum queue length. Unfortunately, the maximum queue length is calculated by the HCS only for minor road flared approaches, which does not address the issue of congestion in the median opening.

## Case Study

The HCS was applied to the same base condition for that used in the CORSIM simulation (Route 13 at Route O in MoDOT's District 8) described in Chapter 4. The HCS application demonstrated both the strengths and weaknesses of the HCM approach. The delay and level of service for each turning movement were estimated with little effort. However, since results are reported by movement, some critical information was absent. For example, the delay experienced by a minor road crossing vehicle consists of delay when waiting for expressway traffic coming from the left (before the minor road vehicle reaches the median) and delay while in the median and waiting for a gap in expressway traffic coming from the right. This division of delay is due to two-stage gap acceptance.

To overcome this problem, the data were manipulated to analyze the crossover location as two separate intersections. While this is mathematically appropriate, it may seem to be an uncomfortable burden to an engineer responsible for the analysis. Unfortunately, no method was found to force the HCS to correctly identify the capacities, delays, or levels of service for the flows. The reason for this flaw in the application was not determined. Due to these problems, the case study was ended.

## EVALUATION

The HCM and HCS can be used to estimate the capacities, delays, or levels of service for the flows at a crossover. Unfortunately, no means was found to apply the HCS to accurately identify the capacities, delays, or levels of service for the flows and queuing vehicles within the median crossover (stage II of the two-stage gap acceptance procedure). However, the expected accuracy and usefulness of this type of approach are discussed below.

## ACCURACY ISSUES AND LIMITATIONS

The HCM assumes a constant vehicle length. At many rural crossovers, problems arise when long trucks are present. Since the HCM deals with average conditions, vehicle length is not explicitly addressed.

The HCM also assumes that critical gap is a constant. If expected queue lengths are long then average delays may also be long. When minor road or major road left-turning traffic experiences long delays, drivers will often accept shorter (and perhaps dangerously short) gaps.

## EASE OF USE

The HCS generally can be applied in a relatively short time. A graduate student who was just learning to apply the HCS found that learning to apply the software required several hours. However, once some experience was gained, he could take a plan view of an intersection and 15-minute count data and, within 15 minutes, have the intersection analyzed by the HCS.

## Conclusions

The HCM and HCS can be used to describe average flow conditions for individual movements (i.e., lefts, throughs, and rights) at a crossover. One can usually take HCS results and manually estimate $95^{\text {th }}$ percentile queue lengths. However the analysts were unable to force the HCS to accurately estimate the delays taking place within the median crossover. For this reason, the HCS proved to be a weaker tool than needed for analyzing crossovers.

## VI. COST ESTIMATES FOR EVALUATION

There exist several approaches to evaluating alternative improvements. All require some sort of cost information. The purpose of this brief chapter is to propose one method for estimating capital costs using the Case 3 alternative described in Chapter 4. MoDOT construction cost data were used to develop the costs of improvements.

## COST ESTIMATES

The "big cost" items were assumed to be those listed in Table 6.1 and were the only ones included in cost estimates.

Table 6.1 MoDOT Unit Costs

| Item Number | Description | Unit cost | Unit |
| :---: | :--- | ---: | :---: |
| $201-10.00$ | Clearing | $\$ 2,340.72$ | ACRE |
| $201-20.00$ | Grubbing | $\$ 1,807.37$ | ACRE |
| $203-50.00$ | Unclassified Excavation | $\$$ | 2.69 |
| $403-81.30$ | AC PG64-28 | CY |  |
| $304-00.43$ | Aggregate base | $\$$ | 117.80 |
| $310-50.01$ | Gravel (for sub-base) | $\$$ | 26.54 |
| $620-55.18$ | Thermoplastic 8 " lines | CY |  |
| $620-55.19$ | Thermoplastic ONLY | $\$$ | 1.14 |
| $903-50.09$ | Stop Sign $(36 ")$ | LF |  |
| $903-50.04$ | Signage | $\$$ | 124.25 |
| $903-12.40$ | Breakaway assembly | $\$ 161.71$ | EA |
|  | $\$$ | 22.71 | SF |

All calculations are based upon the following assumptions:

- Width of repair zone between improved and existing pavements equals 5 ft .,
- Depth of excavation equals 1.5 ft .,
- Pavement structure consists of 4 in. AC, 4 in. granular base, 12 in. gravel sub-base,
- New median opening is a Type I crossover design as indicated in MoDOT's standard drawings, and
- Maintenance costs are equal for all of the alternative designs presented in Figures 4.1.

Areas upon which costs are based are shown in Tables 6.2 and 6.3 below and derive from MoDOT's standard drawings for Types I and II crossovers. The following terms are used in the subsequent tables:

## Terms

$\mathrm{Lj}=$ Length of jug handle
$\mathrm{N}=$ number of lanes on jug handle
Length $=$ length of storage lane
$\mathrm{L}_{\mathrm{j}}=450$ (storage in jug approximately 50 ft .)
$\mathrm{N}=1$

Table 6.2 Case 3
a) Total Area to be Excavated in Square Yards (SY)

|  | Length (ft) |  |  |  |  |  |  |  |  |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Width (ft) | $\mathbf{5 0}$ | $\mathbf{7 5}$ | $\mathbf{1 0 0}$ | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | $\mathbf{1 7 5}$ | $\mathbf{2 0 0}$ | $\mathbf{2 2 5}$ | $\mathbf{2 5 0}$ |
| $\mathbf{5 0}$ | 2,239 | 2,311 | 2,383 | 2,455 | 2,527 | 2,599 | 2,671 | 2,743 | 2,815 |
| $\mathbf{5 5}$ | 2,300 | 2,372 | 2,444 | 2,516 | 2,588 | 2,660 | 2,732 | 2,804 | 2,876 |
| $\mathbf{6 0}$ | 2,360 | 2,432 | 2,504 | 2,576 | 2,648 | 2,720 | 2,792 | 2,864 | 2,936 |
| $\mathbf{6 5}$ | 2,421 | 2,493 | 2,565 | 2,637 | 2,709 | 2,781 | 2,853 | 2,925 | 2,997 |
| $\mathbf{7 0}$ | 2,482 | 2,554 | 2,626 | 2,698 | 2,770 | 2,842 | 2,914 | 2,986 | 3,058 |
| $\mathbf{7 5}$ | 2,542 | 2,614 | 2,686 | 2,758 | 2,830 | 2,902 | 2,974 | 3,046 | 3,118 |
| $\mathbf{8 0}$ | 2,603 | 2,675 | 2,747 | 2,819 | 2,891 | 2,963 | 3,035 | 3,107 | 3,179 |
| $\mathbf{8 5}$ | 2,663 | 2,735 | 2,807 | 2,879 | 2,951 | 3,023 | 3,095 | 3,167 | 3,239 |
| $\mathbf{9 0}$ | 2,724 | 2,796 | 2,868 | 2,940 | 3,012 | 3,084 | 3,156 | 3,228 | 3,300 |
| $\mathbf{9 5}$ | 2,785 | 2,857 | 2,929 | 3,001 | 3,073 | 3,145 | 3,217 | 3,289 | 3,361 |
| $\mathbf{1 0 0}$ | 2,845 | 2,917 | 2,989 | 3,061 | 3,133 | 3,205 | 3,277 | 3,349 | 3,421 |

b) Areas to be Paved in Square Yards (SY)

| Width | Length (ft) |  |  |  |  |  |  |  |  |  | $\mathbf{5 0}$ | $\mathbf{7 5}$ | $\mathbf{1 0 0}$ | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | $\mathbf{1 7 5}$ | $\mathbf{2 0 0}$ | $\mathbf{2 2 5}$ | $\mathbf{2 5 0}$ |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 992 | 1,020 | 1,048 | 1,075 | 1,103 | 1,130 | 1,158 | 1,185 | 1,213 |  |  |  |  |  |  |  |  |  |  |
|  | 1,015 | 1,043 | 1,070 | 1,098 | 1,125 | 1,153 | 1,180 | 1,208 | 1,235 |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{6 0}$ | 1,038 | 1,065 | 1,093 | 1,120 | 1,148 | 1,175 | 1,203 | 1,231 | 1,258 |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{6 5}$ | 1,060 | 1,088 | 1,115 | 1,143 | 1,170 | 1,198 | 1,226 | 1,253 | 1,281 |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{7 0}$ | 1,083 | 1,110 | 1,138 | 1,165 | 1,193 | 1,221 | 1,248 | 1,276 | 1,303 |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{7 5}$ | 1,105 | 1,133 | 1,160 | 1,188 | 1,216 | 1,243 | 1,271 | 1,298 | 1,326 |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{8 0}$ | 1,128 | 1,156 | 1,183 | 1,211 | 1,238 | 1,266 | 1,293 | 1,321 | 1,348 |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{8 5}$ | 1,151 | 1,178 | 1,206 | 1,233 | 1,261 | 1,288 | 1,316 | 1,343 | 1,371 |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{9 0}$ | 1,173 | 1,201 | 1,228 | 1,256 | 1,283 | 1,311 | 1,338 | 1,366 | 1,394 |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{9 5}$ | 1,196 | 1,223 | 1,251 | 1,278 | 1,306 | 1,333 | 1,361 | 1,389 | 1,416 |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{1 0 0}$ | 1,218 | 1,246 | 1,273 | 1,301 | 1,329 | 1,356 | 1,384 | 1,411 | 1,439 |  |  |  |  |  |  |  |  |  |  |

## c) Total Costs for Alternative

| Width <br> (ft) | Length (ft) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 50 | 75 |  | 100 |  | 125 |  | 150 |  | 175 |  | 200 |  | 225 |  | 250 |  |
| 50 | \$ 51,635 | \$ | 52,919 | \$ | 54,204 | S | 55,488 | \$ | 56,772 | \$ | 58,057 | \$ | 59,341 | \$ | 60,625 |  | 61,910 |
| 55 | \$ 52,656 | \$ | 53,940 | \$ | 55,224 | \$ | 56,509 | \$ | 57,793 | \$ | 59,077 | \$ | 60,362 | \$ | 61,646 |  | 62,930 |
| 60 | \$ 53,677 | \$ | 54,961 | \$ | 56,245 | \$ | 57,530 | \$ | 58,814 | \$ | 60,098 | \$ | 61,383 | \$ | 62,667 | S | 63,951 |
| 65 | \$ 54,697 | \$ | 55,982 | \$ | 57,266 | \$ | 58,550 | \$ | 59,835 | \$ | 61,119 | \$ | 62,403 | \$ | 63,688 | \$ | 64,972 |
| 70 | \$ 55,718 | \$ | 57,003 | \$ | 58,287 | \$ | 59,571 | \$ | 60,856 | \$ | 62,140 | \$ | 63,424 | \$ | 64,708 | \$ | 65,993 |
| 75 | \$ 56,739 | \$ | 58,023 | \$ | 59,308 | \$ | 60,592 | \$ | 61,876 | \$ | 63,161 | \$ | 64,445 | \$ | 65,729 | \$ | 67,0 |
| 80 | \$ 57,760 | \$ | 59,044 | \$ | 60,328 | \$ | 61,613 | \$ | 62,897 | \$ | 64,181 | \$ | 65,466 | \$ | 66,750 |  | 68,034 |
| 85 | \$ 58,781 | \$ | 60,065 | \$ | 61,349 | \$ | 62,634 | \$ | 63,918 | \$ | 65,202 | \$ | 66,487 | \$ | 67,771 | \$ | 69,055 |
| 90 | \$ 59,801 | \$ | 61,086 | \$ | 62,370 | \$ | 63,654 | \$ | 64,939 | \$ | 66,223 | \$ | 67,507 | \$ | 68,792 | \$ | 70,076 |
| 95 | \$ 60,822 | \$ | 62,106 | \$ | 63,391 | \$ | 64,675 | \$ | 65,959 | \$ | 67,244 | \$ | 68,528 | \$ | 69,812 | \$ | 71,097 |
| 100 | \$ 61,843 | \$ | 63,127 | \$ | 64,412 | \$ | 65,696 | \$ | 66,980 | \$ | 68,265 | \$ | 69,549 | \$ | 70,833 | \$ | 72,118 |

Table 6.3.1 Case $\mathbf{4}-\mathrm{Lj}=450 \mathrm{ft}$., $\mathrm{N}=1$ lane
a) Total Area to be Excavated in Square Yards (SY)

| Width (ft) | Length (ft) |  |  |  |  |  |  |  |  |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathbf{5 0}$ | $\mathbf{7 5}$ | $\mathbf{1 0 0}$ | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | $\mathbf{1 7 5}$ | $\mathbf{2 0 0}$ | $\mathbf{2 2 5}$ | $\mathbf{2 5 0}$ |
|  | 13,595 | 13,667 | 13,739 | 13,811 | 13,883 | 13,955 | 14,027 | 14,099 | 14,171 |
| $\mathbf{5 5}$ | 13,679 | 13,751 | 13,823 | 13,895 | 13,967 | 14,039 | 14,111 | 14,183 | 14,255 |
| $\mathbf{6 0}$ | 13,762 | 13,834 | 13,906 | 13,978 | 14,050 | 14,122 | 14,194 | 14,266 | 14,338 |
| $\mathbf{6 5}$ | 13,845 | 13,917 | 13,989 | 14,061 | 14,133 | 14,205 | 14,277 | 14,349 | 14,421 |
| $\mathbf{7 0}$ | 13,928 | 14,000 | 14,072 | 14,144 | 14,216 | 14,288 | 14,360 | 14,432 | 14,504 |
| $\mathbf{7 5}$ | 14,011 | 14,083 | 14,155 | 14,227 | 14,299 | 14,371 | 14,443 | 14,515 | 14,587 |
| $\mathbf{8 0}$ | 14,095 | 14,167 | 14,239 | 14,311 | 14,383 | 14,455 | 14,527 | 14,599 | 14,671 |
| $\mathbf{8 5}$ | 14,178 | 14,250 | 14,322 | 14,394 | 14,466 | 14,538 | 14,610 | 14,682 | 14,754 |
| $\mathbf{9 0}$ | 14,261 | 14,333 | 14,405 | 14,477 | 14,549 | 14,621 | 14,693 | 14,765 | 14,837 |
| $\mathbf{9 5}$ | 14,344 | 14,416 | 14,488 | 14,560 | 14,632 | 14,704 | 14,776 | 14,848 | 14,920 |
| $\mathbf{1 0 0}$ | 14,427 | 14,499 | 14,571 | 14,643 | 14,715 | 14,787 | 14,859 | 14,931 | 15,003 |

b) Areas to be Paved in Square Yards (SY)

| Width | Length (ft) |  |  |  |  |  |  |  |  |  | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | $\mathbf{1 7 5}$ | $\mathbf{2 0 0}$ | $\mathbf{2 2 5}$ | $\mathbf{2 5 0}$ |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathbf{5 0}$ | $\mathbf{7 5}$ | $\mathbf{1 0 0}$ | $\mathbf{1 2 5}$ |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 12,349 | 12,376 | 12,404 | 12,431 | 12,459 | 12,486 | 12,514 | 12,542 | 12,569 |  |  |  |  |  |  |  |
| $\mathbf{5 5}$ | 12,394 | 12,421 | 12,449 | 12,477 | 12,504 | 12,532 | 12,559 | 12,587 | 12,614 |  |  |  |  |  |  |  |
| $\mathbf{6 0}$ | 12,439 | 12,467 | 12,494 | 12,522 | 12,549 | 12,577 | 12,604 | 12,632 | 12,659 |  |  |  |  |  |  |  |
| $\mathbf{6 5}$ | 12,484 | 12,512 | 12,539 | 12,567 | 12,594 | 12,622 | 12,650 | 12,677 | 12,705 |  |  |  |  |  |  |  |
| $\mathbf{7 0}$ | 12,529 | 12,557 | 12,584 | 12,612 | 12,640 | 12,667 | 12,695 | 12,722 | 12,750 |  |  |  |  |  |  |  |
| $\mathbf{7 5}$ | 12,575 | 12,602 | 12,630 | 12,657 | 12,685 | 12,712 | 12,740 | 12,767 | 12,795 |  |  |  |  |  |  |  |
| $\mathbf{8 0}$ | 12,620 | 12,647 | 12,675 | 12,702 | 12,730 | 12,757 | 12,785 | 12,813 | 12,840 |  |  |  |  |  |  |  |
| $\mathbf{8 5}$ | 12,665 | 12,692 | 12,720 | 12,748 | 12,775 | 12,803 | 12,830 | 12,858 | 12,885 |  |  |  |  |  |  |  |
| $\mathbf{9 0}$ | 12,710 | 12,738 | 12,765 | 12,793 | 12,820 | 12,848 | 12,875 | 12,903 | 12,930 |  |  |  |  |  |  |  |
| $\mathbf{9 5}$ | 12,755 | 12,783 | 12,810 | 12,838 | 12,865 | 12,893 | 12,921 | 12,948 | 12,976 |  |  |  |  |  |  |  |
| $\mathbf{1 0 0}$ | 12,800 | 12,828 | 12,855 | 12,883 | 12,911 | 12,938 | 12,966 | 12,993 | 13,021 |  |  |  |  |  |  |  |

## c) Total Costs for Alternative

| Width (ft) | Length (ft) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 50 | 75 | 100 | 125 | 150 | 175 | 200 | 225 | 250 |
| 50 | \$ 524,131 | \$ 525,415 | \$ 526,699 | \$ 527,984 | \$ 529,268 | \$ 530,552 | \$ 531,837 | \$ 533,121 | \$ 534,405 |
| 55 | \$ 526,077 | \$ 527,361 | \$ 528,646 | \$ 529,930 | \$ 531,214 | \$ 532,499 | \$ 533,783 | \$ 535,067 | \$ 536,352 |
| 60 | \$ 528,024 | \$ 529,308 | \$ 530,592 | \$ 531,876 | \$ 533,161 | \$ 534,445 | \$ 535,729 | \$ 537,014 | \$ 538,298 |
| 65 | \$ 529,970 | \$ 531,254 | \$ 532,539 | \$ 533,823 | \$ 535,107 | \$ 536,392 | \$ 537,676 | \$ 538,960 | \$ 540,245 |
| 70 | \$ 531,916 | \$ 533,201 | \$ 534,485 | \$ 535,769 | \$ 537,054 | \$ 538,338 | \$ 539,622 | \$ 540,907 | \$ 542,191 |
| 75 | \$ 533,863 | \$ 535,147 | \$ 536,431 | \$ 537,716 | \$ 539,000 | \$ 540,284 | \$ 541,569 | \$ 542,853 | \$ 544,137 |
| 80 | \$ 535,809 | \$ 537,094 | \$ 538,378 | \$ 539,662 | \$ 540,947 | \$ 542,231 | \$ 543,515 | \$ 544,800 | \$ 546,084 |
| 85 | \$ 537,756 | \$ 539,040 | \$ 540,324 | \$ 541,609 | \$ 542,893 | \$ 544,177 | \$ 545,462 | \$ 546,746 | \$ 548,030 |
| 90 | \$ 539,702 | \$ 540,986 | \$ 542,271 | \$ 543,555 | \$ 544,839 | \$ 546,124 | \$ 547,408 | \$ 548,692 | \$ 549,977 |
| 95 | \$ 541,649 | \$ 542,933 | \$ 544,217 | \$ 545,502 | \$ 546,786 | \$ 548,070 | \$ 549,355 | \$ 550,639 | \$ 551,923 |
| 100 | \$ 543,595 | \$ 544,879 | \$ 546,164 | \$ 547,448 | \$ 548,732 | \$ 550,017 | \$ 551,301 | \$ 552,585 | \$ 553,870 |

Table 6.3.2 Case $\mathbf{4} \mathbf{- L j}=450 \mathrm{ft}$., $\mathrm{N}=2$ lanes
a) Total Area to be Excavated in Square Yards (SY)

| Width (ft) | Length (ft) |  |  |  |  |  |  |  |  |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathbf{5 0}$ | $\mathbf{7 5}$ | $\mathbf{1 0 0}$ | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | $\mathbf{1 7 5}$ | $\mathbf{2 0 0}$ | $\mathbf{2 2 5}$ | $\mathbf{2 5 0}$ |
|  | 24,425 | 24,497 | 24,569 | 24,641 | 24,713 | 24,785 | 24,857 | 24,929 | 25,001 |
| $\mathbf{5 5}$ | 24,509 | 24,581 | 24,653 | 24,725 | 24,797 | 24,869 | 24,941 | 25,013 | 25,085 |
| $\mathbf{6 0}$ | 24,592 | 24,664 | 24,736 | 24,808 | 24,880 | 24,952 | 25,024 | 25,096 | 25,168 |
| $\mathbf{6 5}$ | 24,675 | 24,747 | 24,819 | 24,891 | 24,963 | 25,035 | 25,107 | 25,179 | 25,251 |
| $\mathbf{7 0}$ | 24,758 | 24,830 | 24,902 | 24,974 | 25,046 | 25,118 | 25,190 | 25,262 | 25,334 |
| $\mathbf{7 5}$ | 24,841 | 24,913 | 24,985 | 25,057 | 25,129 | 25,201 | 25,273 | 25,345 | 25,417 |
| $\mathbf{8 0}$ | 24,925 | 24,997 | 25,069 | 25,141 | 25,213 | 25,285 | 25,357 | 25,429 | 25,501 |
| $\mathbf{8 5}$ | 25,008 | 25,080 | 25,152 | 25,224 | 25,296 | 25,368 | 25,440 | 25,512 | 25,584 |
| $\mathbf{9 0}$ | 25,091 | 25,163 | 25,235 | 25,307 | 25,379 | 25,451 | 25,523 | 25,595 | 25,667 |
| $\mathbf{9 5}$ | 25,174 | 25,246 | 25,318 | 25,390 | 25,462 | 25,534 | 25,606 | 25,678 | 25,750 |
| $\mathbf{1 0 0}$ | 25,257 | 25,329 | 25,401 | 25,473 | 25,545 | 25,617 | 25,689 | 25,761 | 25,833 |

b) Areas to be Paved in Square Yards (SY)

| Width | $\mathbf{5 0}$ | $\mathbf{7 5}$ | $\mathbf{1 0 0}$ | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | $\mathbf{1 7 5}$ | $\mathbf{2 0 0}$ | $\mathbf{2 2 5}$ | $\mathbf{2 5 0}$ |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathbf{5 0}$ | 23,179 | 23,206 | 23,234 | 23,261 | 23,289 | 23,316 | 23,344 | 23,372 |
| $\mathbf{5 5}$ | 23,224 | 23,251 | 23,279 | 23,307 | 23,334 | 23,362 | 23,389 | 23,417 | 23,444 |
| $\mathbf{6 0}$ | 23,269 | 23,297 | 23,324 | 23,352 | 23,379 | 23,407 | 23,434 | 23,462 | 23,489 |
| $\mathbf{6 5}$ | 23,314 | 23,342 | 23,369 | 23,397 | 23,424 | 23,452 | 23,480 | 23,507 | 23,535 |
| $\mathbf{7 0}$ | 23,359 | 23,387 | 23,414 | 23,442 | 23,470 | 23,497 | 23,525 | 23,552 | 23,580 |
| $\mathbf{7 5}$ | 23,405 | 23,432 | 23,460 | 23,487 | 23,515 | 23,542 | 23,570 | 23,597 | 23,625 |
| $\mathbf{8 0}$ | 23,450 | 23,477 | 23,505 | 23,532 | 23,560 | 23,587 | 23,615 | 23,643 | 23,670 |
| $\mathbf{8 5}$ | 23,495 | 23,522 | 23,550 | 23,578 | 23,605 | 23,633 | 23,660 | 23,688 | 23,715 |
| $\mathbf{9 0}$ | 23,540 | 23,568 | 23,595 | 23,623 | 23,650 | 23,678 | 23,705 | 23,733 | 23,760 |
| $\mathbf{9 5}$ | 23,585 | 23,613 | 23,640 | 23,668 | 23,695 | 23,723 | 23,751 | 23,778 | 23,806 |
| $\mathbf{1 0 0}$ | 23,630 | 23,658 | 23,685 | 23,713 | 23,741 | 23,768 | 23,796 | 23,823 | 23,851 |

## c) Total Costs for Alternative

| Width (ft) | Length (ft) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 50 |  | 75 |  | 100 |  | 125 |  | 150 |  | 175 |  | 200 |  | 225 |  | 250 |
| 50 | \$ | 968,547 | \$ | 969,831 | \$ | 971,116 | \$ | 972,400 | \$ | 973,684 | \$ | 974,969 | \$ | 976,253 | \$ | 977,537 | \$ | 978,822 |
| 55 | \$ | 970,493 | \$ | 971,778 | \$ | 973,062 | \$ | 974,346 | \$ | 975,631 | \$ | 976,915 | \$ | 978,199 | \$ | 979,484 | \$ | 980,768 |
| 60 | \$ | 972,440 | \$ | 973,724 | \$ | 975,009 | \$ | 976,293 | \$ | 977,577 | \$ | 978,862 | \$ | 980,146 | \$ | 981,430 | S | 982,715 |
| 65 | \$ | 974,386 | \$ | 975,671 | \$ | 976,955 | \$ | 978,239 | \$ | 979,524 | \$ | 980,808 | \$ | 982,092 | \$ | 983,377 | \$ | 984,661 |
| 70 | \$ | 976,333 | \$ | 977,617 | \$ | 978,901 | \$ | 980,186 | \$ | 981,470 | \$ | 982,754 | \$ | 984,039 | \$ | 985,323 | \$ | 986,607 |
| 75 | \$ | 978,279 | \$ | 979,564 | \$ | 980,848 | \$ | 982,132 | \$ | 983,417 | \$ | 984,701 | \$ | 985,985 | \$ | 987,269 | \$ | 988,554 |
| 80 | \$ | 980,226 | \$ | 981,510 | \$ | 982,794 | \$ | 984,079 | \$ | 985,363 | \$ | 986,647 | \$ | 987,932 | \$ | 989,216 | \$ | 990,500 |
| 85 | \$ | 982,172 | \$ | 983,456 | \$ | 984,741 | \$ | 986,025 | \$ | 987,309 | \$ | 988,594 | \$ | 989,878 | \$ | 991,162 | \$ | 992,447 |
| 90 | \$ | 984,119 | \$ | 985,403 | \$ | 986,687 | \$ | 987,972 | \$ | 989,256 | \$ | 990,540 | \$ | 991,824 | \$ | 993,109 | \$ | 994,393 |
| 95 | \$ | 986,065 | \$ | 987,349 | \$ | 988,634 | \$ | 989,918 | \$ | 991,202 | \$ | 992,487 | \$ | 993,771 | \$ | 995,055 | \$ | 996,340 |
| 100 | \$ | 988,011 | \$ | 989,296 | \$ | 990,580 | \$ | 991,864 | \$ | 993,149 | \$ | 994,433 | \$ | 995,717 | \$ | 997,002 | \$ | 998,286 |

Table 6.3.3 Case $\mathbf{4}-\mathrm{Lj}=550 \mathrm{ft}$., $\mathrm{N}=1$ lane
a) Total Area to be Excavated in Square Yards (SY)

| Width (ft) | Length (ft) |  |  |  |  |  |  |  |  |  |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathbf{5 0}$ | $\mathbf{7 5}$ | $\mathbf{1 0 0}$ | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | $\mathbf{1 7 5}$ | $\mathbf{2 0 0}$ | $\mathbf{2 2 5}$ | $\mathbf{2 5 0}$ |  |
|  | 15,995 | 16,067 | 16,139 | 16,211 | 16,283 | 16,355 | 16,427 | 16,499 | 16,571 |  |
| $\mathbf{5 5}$ | 16,079 | 16,151 | 16,223 | 16,295 | 16,367 | 16,439 | 16,511 | 16,583 | 16,655 |  |
| $\mathbf{6 0}$ | 16,162 | 16,234 | 16,306 | 16,378 | 16,450 | 16,522 | 16,594 | 16,666 | 16,738 |  |
| $\mathbf{6 5}$ | 16,245 | 16,317 | 16,389 | 16,461 | 16,533 | 16,605 | 16,677 | 16,749 | 16,821 |  |
| $\mathbf{7 0}$ | 16,328 | 16,400 | 16,472 | 16,544 | 16,616 | 16,688 | 16,760 | 16,832 | 16,904 |  |
| $\mathbf{7 5}$ | 16,411 | 16,483 | 16,555 | 16,627 | 16,699 | 16,771 | 16,843 | 16,915 | 16,987 |  |
| $\mathbf{8 0}$ | 16,495 | 16,567 | 16,639 | 16,711 | 16,783 | 16,855 | 16,927 | 16,999 | 17,071 |  |
| $\mathbf{8 5}$ | 16,578 | 16,650 | 16,722 | 16,794 | 16,866 | 16,938 | 17,010 | 17,082 | 17,154 |  |
| $\mathbf{9 0}$ | 16,661 | 16,733 | 16,805 | 16,877 | 16,949 | 17,021 | 17,093 | 17,165 | 17,237 |  |
| $\mathbf{9 5}$ | 16,744 | 16,816 | 16,888 | 16,960 | 17,032 | 17,104 | 17,176 | 17,248 | 17,320 |  |
| $\mathbf{1 0 0}$ | 16,827 | 16,899 | 16,971 | 17,043 | 17,115 | 17,187 | 17,259 | 17,331 | 17,403 |  |

b) Areas to be Paved in Square Yards (SY)

| Width | Length (ft) |  |  |  |  |  |  |  |  |  | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | $\mathbf{1 7 5}$ | $\mathbf{2 0 0}$ | $\mathbf{2 2 5}$ | $\mathbf{2 5 0}$ |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathbf{5 0}$ | $\mathbf{7 5}$ | $\mathbf{1 0 0}$ | $\mathbf{1 2 5}$ |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 14,749 | 14,776 | 14,804 | 14,831 | 14,859 | 14,886 | 14,914 | 14,942 | 14,969 |  |  |  |  |  |  |  |
| $\mathbf{5 5}$ | 14,794 | 14,821 | 14,849 | 14,877 | 14,904 | 14,932 | 14,959 | 14,987 | 15,014 |  |  |  |  |  |  |  |
| $\mathbf{6 0}$ | 14,839 | 14,867 | 14,894 | 14,922 | 14,949 | 14,977 | 15,004 | 15,032 | 15,059 |  |  |  |  |  |  |  |
| $\mathbf{6 5}$ | 14,884 | 14,912 | 14,939 | 14,967 | 14,994 | 15,022 | 15,050 | 15,077 | 15,105 |  |  |  |  |  |  |  |
| $\mathbf{7 0}$ | 14,929 | 14,957 | 14,984 | 15,012 | 15,040 | 15,067 | 15,095 | 15,122 | 15,150 |  |  |  |  |  |  |  |
| $\mathbf{7 5}$ | 14,975 | 15,002 | 15,030 | 15,057 | 15,085 | 15,112 | 15,140 | 15,167 | 15,195 |  |  |  |  |  |  |  |
| $\mathbf{8 0}$ | 15,020 | 15,047 | 15,075 | 15,102 | 15,130 | 15,157 | 15,185 | 15,213 | 15,240 |  |  |  |  |  |  |  |
| $\mathbf{8 5}$ | 15,065 | 15,092 | 15,120 | 15,148 | 15,175 | 15,203 | 15,230 | 15,258 | 15,285 |  |  |  |  |  |  |  |
| $\mathbf{9 0}$ | 15,110 | 15,138 | 15,165 | 15,193 | 15,220 | 15,248 | 15,275 | 15,303 | 15,330 |  |  |  |  |  |  |  |
| $\mathbf{9 5}$ | 15,155 | 15,183 | 15,210 | 15,238 | 15,265 | 15,293 | 15,321 | 15,348 | 15,376 |  |  |  |  |  |  |  |
| $\mathbf{1 0 0}$ | 15,200 | 15,228 | 15,255 | 15,283 | 15,311 | 15,338 | 15,366 | 15,393 | 15,421 |  |  |  |  |  |  |  |

c) Total Costs for Alternative


Table 6.3.4 Case $\mathbf{4} \mathbf{- L j}=550 \mathrm{ft}$., $\mathrm{N}=2$ lanes
a) Total Area to be Excavated in Square Yards (SY)

| Width (ft) | Length (ft) |  |  |  |  |  |  |  | $\mathbf{5 0}$ |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathbf{7 5}$ | $\mathbf{1 0 0}$ | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | $\mathbf{1 7 5}$ | $\mathbf{2 0 0}$ | $\mathbf{2 2 5}$ | $\mathbf{2 5 0}$ |  |
|  | 29,225 | 29,297 | 29,369 | 29,441 | 29,513 | 29,585 | 29,657 | 29,729 | 29,801 |
| $\mathbf{5 5}$ | 29,309 | 29,381 | 29,453 | 29,525 | 29,597 | 29,669 | 29,741 | 29,813 | 29,885 |
| $\mathbf{6 0}$ | 29,392 | 29,464 | 29,536 | 29,608 | 29,680 | 29,752 | 29,824 | 29,896 | 29,968 |
| $\mathbf{6 5}$ | 29,475 | 29,547 | 29,619 | 29,691 | 29,763 | 29,835 | 29,907 | 29,979 | 30,051 |
| $\mathbf{7 0}$ | 29,558 | 29,630 | 29,702 | 29,774 | 29,846 | 29,918 | 29,990 | 30,062 | 30,134 |
| $\mathbf{7 5}$ | 29,641 | 29,713 | 29,785 | 29,857 | 29,929 | 30,001 | 30,073 | 30,145 | 30,217 |
| $\mathbf{8 0}$ | 29,725 | 29,797 | 29,869 | 29,941 | 30,013 | 30,085 | 30,157 | 30,229 | 30,301 |
| $\mathbf{8 5}$ | 29,808 | 29,880 | 29,952 | 30,024 | 30,096 | 30,168 | 30,240 | 30,312 | 30,384 |
| $\mathbf{9 0}$ | 29,891 | 29,963 | 30,035 | 30,107 | 30,179 | 30,251 | 30,323 | 30,395 | 30,467 |
| $\mathbf{9 5}$ | 29,974 | 30,046 | 30,118 | 30,190 | 30,262 | 30,334 | 30,406 | 30,478 | 30,550 |
| $\mathbf{1 0 0}$ | 30,057 | 30,129 | 30,201 | 30,273 | 30,345 | 30,417 | 30,489 | 30,561 | 30,633 |

b) Areas to be Paved in Square Yards (SY)

| Width | $\mathbf{5 0}$ | $\mathbf{7 5}$ | $\mathbf{1 0 0}$ | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | $\mathbf{1 7 5}$ | $\mathbf{2 0 0}$ | $\mathbf{2 2 5}$ | $\mathbf{2 5 0}$ |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathbf{5 0}$ | 27,979 | 28,006 | 28,034 | 28,061 | 28,089 | 28,116 | 28,144 | 28,172 |
| $\mathbf{5 5}$ | 28,024 | 28,051 | 28,079 | 28,107 | 28,134 | 28,162 | 28,189 | 28,217 | 28,244 |
| $\mathbf{6 0}$ | 28,069 | 28,097 | 28,124 | 28,152 | 28,179 | 28,207 | 28,234 | 28,262 | 28,289 |
| $\mathbf{6 5}$ | 28,114 | 28,142 | 28,169 | 28,197 | 28,224 | 28,252 | 28,280 | 28,307 | 28,335 |
| $\mathbf{7 0}$ | 28,159 | 28,187 | 28,214 | 28,242 | 28,270 | 28,297 | 28,325 | 28,352 | 28,380 |
| $\mathbf{7 5}$ | 28,205 | 28,232 | 28,260 | 28,287 | 28,315 | 28,342 | 28,370 | 28,397 | 28,425 |
| $\mathbf{8 0}$ | 28,250 | 28,277 | 28,305 | 28,332 | 28,360 | 28,387 | 28,415 | 28,443 | 28,470 |
| $\mathbf{8 5}$ | 28,295 | 28,322 | 28,350 | 28,378 | 28,405 | 28,433 | 28,460 | 28,488 | 28,515 |
| $\mathbf{9 0}$ | 28,340 | 28,368 | 28,395 | 28,423 | 28,450 | 28,478 | 28,505 | 28,533 | 28,560 |
| $\mathbf{9 5}$ | 28,385 | 28,413 | 28,440 | 28,468 | 28,495 | 28,523 | 28,551 | 28,578 | 28,606 |
| $\mathbf{1 0 0}$ | 28,430 | 28,458 | 28,485 | 28,513 | 28,541 | 28,568 | 28,596 | 28,623 | 28,651 |

## c) Total Costs for Alternative

|  | Length (ft) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Width (ft) | 50 | 75 | 100 | 125 | 150 | 175 | 200 | 225 | 250 |
| 50 | \$ 1,165,633 | \$ 1,166,917 | \$ 1,168,202 | \$ 1,169,486 | \$ 1,170,770 | \$ 1,172,055 | \$ 1,173,339 | \$ 1,174,623 | \$ 1,175,908 |
| 55 | \$ 1,167,579 | \$ 1,168,864 | \$ 1,170,148 | \$ 1,171,432 | \$ 1,172,717 | \$ 1,174,001 | \$ 1,175,285 | \$ 1,176,570 | \$ 1,177,854 |
| 60 | \$ 1,169,526 | \$ 1,170,810 | \$ 1,172,094 | \$ 1,173,379 | \$ 1,174,663 | \$ 1,175,947 | \$ 1,177,232 | \$ 1,178,516 | \$ 1,179,800 |
| 65 | \$ 1,171,472 | \$ 1,172,757 | \$ 1,174,041 | \$ 1,175,325 | \$ 1,176,610 | \$ 1,177,894 | \$ 1,179,178 | \$ 1,180,463 | \$ 1,181,747 |
| 70 | \$ 1,173,419 | \$ 1,174,703 | \$ 1,175,987 | \$ 1,177,272 | \$ 1,178,556 | \$ 1,179,840 | \$ 1,181,125 | \$ 1,182,409 | \$ 1,183,693 |
| 75 | \$ 1,175,365 | \$ 1,176,649 | \$ 1,177,934 | \$ 1,179,218 | \$ 1,180,502 | \$ 1,181,787 | \$ 1,183,071 | \$ 1,184,355 | \$ 1,185,640 |
| 80 | \$ 1,177,312 | \$ 1,178,596 | \$ 1,179,880 | \$ 1,181,165 | \$ 1,182,449 | \$ 1,183,733 | \$ 1,185,018 | \$ 1,186,302 | \$ 1,187,586 |
| 85 | \$ 1,179,258 | \$ 1,180,542 | \$ 1,181,827 | \$ 1,183,111 | \$ 1,184,395 | \$ 1,185,680 | \$ 1,186,964 | \$ 1,188,248 | \$ 1,189,533 |
| 90 | \$ 1,181,204 | \$ 1,182,489 | \$ 1,183,773 | \$ 1,185,057 | \$ 1,186,342 | \$ 1,187,626 | \$ 1,188,910 | \$ 1,190,195 | \$ 1,191,479 |
| 95 | \$ 1,183,151 | \$ 1,184,435 | \$ 1,185,720 | \$ 1,187,004 | \$ 1,188,288 | \$ 1,189,572 | \$ 1,190,857 | \$ 1,192,141 | \$ 1,193,425 |
| 100 | \$ 1,185,097 | \$ 1,186,382 | \$ 1,187,666 | \$ 1,188,950 | \$ 1,190,235 | \$ 1,191,519 | \$ 1,192,803 | \$ 1,194,088 | \$ 1,195,372 |

Table 6.3.5 Case $4-\mathrm{Lj}=650 \mathrm{ft}$., $\mathrm{N}=1$ lane
a) Total Area to be Excavated in Square Yards (SY)

| Width (ft) | Length (ft) |  |  |  |  |  |  |  |  |  |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathbf{5 0}$ | $\mathbf{7 5}$ | $\mathbf{1 0 0}$ | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | $\mathbf{1 7 5}$ | $\mathbf{2 0 0}$ | $\mathbf{2 2 5}$ | $\mathbf{2 5 0}$ |  |
|  | 18,395 | 18,467 | 18,539 | 18,611 | 18,683 | 18,755 | 18,827 | 18,899 | 18,971 |  |
| $\mathbf{5 5}$ | 18,479 | 18,551 | 18,623 | 18,695 | 18,767 | 18,839 | 18,911 | 18,983 | 19,055 |  |
| $\mathbf{6 0}$ | 18,562 | 18,634 | 18,706 | 18,778 | 18,850 | 18,922 | 18,994 | 19,066 | 19,138 |  |
| $\mathbf{6 5}$ | 18,645 | 18,717 | 18,789 | 18,861 | 18,933 | 19,005 | 19,077 | 19,149 | 19,221 |  |
| $\mathbf{7 0}$ | 18,728 | 18,800 | 18,872 | 18,944 | 19,016 | 19,088 | 19,160 | 19,232 | 19,304 |  |
| $\mathbf{7 5}$ | 18,811 | 18,883 | 18,955 | 19,027 | 19,099 | 19,171 | 19,243 | 19,315 | 19,387 |  |
| $\mathbf{8 0}$ | 18,895 | 18,967 | 19,039 | 19,111 | 19,183 | 19,255 | 19,327 | 19,399 | 19,471 |  |
| $\mathbf{8 5}$ | 18,978 | 19,050 | 19,122 | 19,194 | 19,266 | 19,338 | 19,410 | 19,482 | 19,554 |  |
| $\mathbf{9 0}$ | 19,061 | 19,133 | 19,205 | 19,277 | 19,349 | 19,421 | 19,493 | 19,565 | 19,637 |  |
| $\mathbf{9 5}$ | 19,144 | 19,216 | 19,288 | 19,360 | 19,432 | 19,504 | 19,576 | 19,648 | 19,720 |  |
| $\mathbf{1 0 0}$ | 19,227 | 19,299 | 19,371 | 19,443 | 19,515 | 19,587 | 19,659 | 19,731 | 19,803 |  |

b) Areas to be Paved in Square Yards (SY)

| Width | Length (ft) |  |  |  |  |  |  |  |  |  | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | $\mathbf{1 7 5}$ | $\mathbf{2 0 0}$ | $\mathbf{2 2 5}$ | $\mathbf{2 5 0}$ |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathbf{5 0}$ | $\mathbf{7 5}$ | $\mathbf{1 0 0}$ | $\mathbf{1 2 5}$ |  |  |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{5 0}$ | 17,149 | 17,176 | 17,204 | 17,231 | 17,259 | 17,286 | 17,314 | 17,342 | 17,369 |  |  |  |  |  |  |  |
| $\mathbf{5 5}$ | 17,194 | 17,221 | 17,249 | 17,277 | 17,304 | 17,332 | 17,359 | 17,387 | 17,414 |  |  |  |  |  |  |  |
| $\mathbf{6 0}$ | 17,239 | 17,267 | 17,294 | 17,322 | 17,349 | 17,377 | 17,404 | 17,432 | 17,459 |  |  |  |  |  |  |  |
| $\mathbf{6 5}$ | 17,284 | 17,312 | 17,339 | 17,367 | 17,394 | 17,422 | 17,450 | 17,477 | 17,505 |  |  |  |  |  |  |  |
| $\mathbf{7 0}$ | 17,329 | 17,357 | 17,384 | 17,412 | 17,440 | 17,467 | 17,495 | 17,522 | 17,550 |  |  |  |  |  |  |  |
| $\mathbf{7 5}$ | 17,375 | 17,402 | 17,430 | 17,457 | 17,485 | 17,512 | 17,540 | 17,567 | 17,595 |  |  |  |  |  |  |  |
| $\mathbf{8 0}$ | 17,420 | 17,447 | 17,475 | 17,502 | 17,530 | 17,557 | 17,585 | 17,613 | 17,640 |  |  |  |  |  |  |  |
| $\mathbf{8 5}$ | 17,465 | 17,492 | 17,520 | 17,548 | 17,575 | 17,603 | 17,630 | 17,658 | 17,685 |  |  |  |  |  |  |  |
| $\mathbf{9 0}$ | 17,510 | 17,538 | 17,565 | 17,593 | 17,620 | 17,648 | 17,675 | 17,703 | 17,730 |  |  |  |  |  |  |  |
| $\mathbf{9 5}$ | 17,555 | 17,583 | 17,610 | 17,638 | 17,665 | 17,693 | 17,721 | 17,748 | 17,776 |  |  |  |  |  |  |  |
| $\mathbf{1 0 0}$ | 17,600 | 17,628 | 17,655 | 17,683 | 17,711 | 17,738 | 17,766 | 17,793 | 17,821 |  |  |  |  |  |  |  |

## c) Total Costs for Alternative

| Width (ft) | Length (ft) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 50 |  | 75 |  | 100 |  | 125 |  | 150 |  | 175 |  | 200 |  | 225 |  | 250 |  |
| 50 | \$ | 721,331 | \$ | 722,615 | \$ | 723,899 | \$ | 725,184 | \$ | 726,468 | \$ | 727,752 | \$ | 729,036 | \$ | 730,321 | \$ | 731,605 |
| 55 | \$ | 723,277 | \$ | 724,561 | \$ | 725,846 | \$ | 727,130 | \$ | 728,414 | \$ | 729,699 | \$ | 730,983 | \$ | 732,267 | \$ | 733,552 |
| 60 | \$ | 725,223 | \$ | 726,508 | \$ | 727,792 | \$ | 729,076 | \$ | 730,361 | \$ | 731,645 | \$ | 732,929 | \$ | 734,214 | \$ | 735,498 |
| 65 | \$ | 727,170 | \$ | 728,454 | \$ | 729,738 | \$ | 731,023 | \$ | 732,307 | \$ | 733,591 | \$ | 734,876 | \$ | 736,160 | \$ | 737,444 |
| 70 | \$ | 729,116 | \$ | 730,401 | \$ | 731,685 | \$ | 732,969 | \$ | 734,254 | \$ | 735,538 | \$ | 736,822 | \$ | 738,107 | \$ | 739,391 |
| 75 | \$ | 731,063 | \$ | 732,347 | \$ | 733,631 | \$ | 734,916 | \$ | 736,200 | \$ | 737,484 | \$ | 738,769 | \$ | 740,053 | \$ | 741,337 |
| 80 | \$ | 733,009 | \$ | 734,293 | \$ | 735,578 | \$ | 736,862 | \$ | 738,146 | \$ | 739,431 | \$ | 740,715 | \$ | 741,999 | \$ | 743,284 |
| 85 | \$ | 734,956 | \$ | 736,240 | \$ | 737,524 | \$ | 738,809 | \$ | 740,093 | \$ | 741,377 | \$ | 742,662 | \$ | 743,946 | \$ | 745,230 |
| 90 | \$ | 736,902 | \$ | 738,186 | \$ | 739,471 | \$ | 740,755 | \$ | 742,039 | \$ | 743,324 | \$ | 744,608 | \$ | 745,892 | \$ | 747,177 |
| 95 | \$ | 738,848 | \$ | 740,133 | \$ | 741,417 | \$ | 742,701 | \$ | 743,986 | \$ | 745,270 | \$ | 746,554 | \$ | 747,839 | \$ | 749,123 |
| 100 | \$ | 740,795 | \$ | 742,079 | \$ | 743,364 | \$ | 744,648 | \$ | 745,932 | \$ | 747,217 | \$ | 748,501 | \$ | 749,785 | \$ | 751,070 |

Table 6.3.6 Case $\mathbf{4}-\mathrm{Lj}=\mathbf{6 5 0} \mathrm{ft}$., $\mathrm{N}=2$ lanes
a) Total Area to be Excavated in Square Yards (SY)

| Width (ft) | Length (ft) |  |  |  |  |  |  |  |  |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathbf{5 0}$ | $\mathbf{7 5}$ | $\mathbf{1 0 0}$ | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | $\mathbf{1 7 5}$ | $\mathbf{2 0 0}$ | $\mathbf{2 2 5}$ | $\mathbf{2 5 0}$ |
|  | 34,025 | 34,097 | 34,169 | 34,241 | 34,313 | 34,385 | 34,457 | 34,529 | 34,601 |
| $\mathbf{5 5}$ | 34,109 | 34,181 | 34,253 | 34,325 | 34,397 | 34,469 | 34,541 | 34,613 | 34,685 |
| $\mathbf{6 0}$ | 34,192 | 34,264 | 34,336 | 34,408 | 34,480 | 34,552 | 34,624 | 34,696 | 34,768 |
| $\mathbf{6 5}$ | 34,275 | 34,347 | 34,419 | 34,491 | 34,563 | 34,635 | 34,707 | 34,779 | 34,851 |
| $\mathbf{7 0}$ | 34,358 | 34,430 | 34,502 | 34,574 | 34,646 | 34,718 | 34,790 | 34,862 | 34,934 |
| $\mathbf{7 5}$ | 34,441 | 34,513 | 34,585 | 34,657 | 34,729 | 34,801 | 34,873 | 34,945 | 35,017 |
| $\mathbf{8 0}$ | 34,525 | 34,597 | 34,669 | 34,741 | 34,813 | 34,885 | 34,957 | 35,029 | 35,101 |
| $\mathbf{8 5}$ | 34,608 | 34,680 | 34,752 | 34,824 | 34,896 | 34,968 | 35,040 | 35,112 | 35,184 |
| $\mathbf{9 0}$ | 34,691 | 34,763 | 34,835 | 34,907 | 34,979 | 35,051 | 35,123 | 35,195 | 35,267 |
| $\mathbf{9 5}$ | 34,774 | 34,846 | 34,918 | 34,990 | 35,062 | 35,134 | 35,206 | 35,278 | 35,350 |
| $\mathbf{1 0 0}$ | 34,857 | 34,929 | 35,001 | 35,073 | 35,145 | 35,217 | 35,289 | 35,361 | 35,433 |

b) Areas to be Paved in Square Yards (SY)

| Width | Length (ft) |  |  |  |  |  |  |  |  |  |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathbf{5 0}$ | $\mathbf{7 5}$ | $\mathbf{1 0 0}$ | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | $\mathbf{1 7 5}$ | $\mathbf{2 0 0}$ | $\mathbf{2 2 5}$ | $\mathbf{2 5 0}$ |  |
| $\mathbf{5 0}$ | 32,779 | 32,806 | 32,834 | 32,861 | 32,889 | 32,916 | 32,944 | 32,972 | 32,999 |  |
| $\mathbf{5 5}$ | 32,824 | 32,851 | 32,879 | 32,907 | 32,934 | 32,962 | 32,989 | 33,017 | 33,044 |  |
| $\mathbf{6 0}$ | 32,869 | 32,897 | 32,924 | 32,952 | 32,979 | 33,007 | 33,034 | 33,062 | 33,089 |  |
| $\mathbf{6 5}$ | 32,914 | 32,942 | 32,969 | 32,997 | 33,024 | 33,052 | 33,080 | 33,107 | 33,135 |  |
| $\mathbf{7 0}$ | 32,959 | 32,987 | 33,014 | 33,042 | 33,070 | 33,097 | 33,125 | 33,152 | 33,180 |  |
| $\mathbf{7 5}$ | 33,005 | 33,032 | 33,060 | 33,087 | 33,115 | 33,142 | 33,170 | 33,197 | 33,225 |  |
| $\mathbf{8 0}$ | 33,050 | 33,077 | 33,105 | 33,132 | 33,160 | 33,187 | 33,215 | 33,243 | 33,270 |  |
| $\mathbf{8 5}$ | 33,095 | 33,122 | 33,150 | 33,178 | 33,205 | 33,233 | 33,260 | 33,288 | 33,315 |  |
| $\mathbf{9 0}$ | 33,140 | 33,168 | 33,195 | 33,223 | 33,250 | 33,278 | 33,305 | 33,333 | 33,360 |  |
| $\mathbf{9 5}$ | 33,185 | 33,213 | 33,240 | 33,268 | 33,295 | 33,323 | 33,351 | 33,378 | 33,406 |  |
| $\mathbf{1 0 0}$ | 33,230 | 33,258 | 33,285 | 33,313 | 33,341 | 33,368 | 33,396 | 33,423 | 33,451 |  |

c) Total Costs for Alternative

| Width (ft) | Length (ft) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 50 | 75 | 100 | 125 | 150 | 175 | 200 | 225 | 250 |
| 50 | \$ 1,362,719 | \$ 1,364,003 | \$ 1,365,287 | \$ 1,366,572 | \$ 1,367,856 | \$ 1,369,140 | \$ 1,370,425 | \$ 1,371,709 | \$ 1,372,993 |
| 55 | \$ 1,364,665 | \$ 1,365,950 | \$ 1,367,234 | \$ 1,368,518 | \$ 1,369,803 | \$ 1,371,087 | \$ 1,372,371 | \$ 1,373,656 | \$ 1,374,940 |
| 60 | \$ 1,366,612 | \$ 1,367,896 | \$ 1,369,180 | \$ 1,370,465 | \$ 1,371,749 | \$ 1,373,033 | \$ 1,374,318 | \$ 1,375,602 | \$ 1,376,886 |
| 65 | \$ 1,368,558 | \$ 1,369,842 | \$ 1,371,127 | \$ 1,372,411 | \$ 1,373,695 | \$ 1,374,980 | \$ 1,376,264 | \$ 1,377,548 | \$ 1,378,833 |
| 70 | \$ 1,370,505 | \$ 1,371,789 | \$ 1,373,073 | \$ 1,374,358 | \$ 1,375,642 | \$ 1,376,926 | \$ 1,378,211 | \$ 1,379,495 | \$ 1,380,779 |
| 75 | \$ 1,372,451 | \$ 1,373,735 | \$ 1,375,020 | \$ 1,376,304 | \$ 1,377,588 | \$ 1,378,873 | \$ 1,380,157 | \$ 1,381,441 | \$ 1,382,726 |
| 80 | \$ 1,374,397 | \$ 1,375,682 | \$ 1,376,966 | \$ 1,378,250 | \$ 1,379,535 | \$ 1,380,819 | \$ 1,382,103 | \$ 1,383,388 | \$ 1,384,672 |
| 85 | \$ 1,376,344 | \$ 1,377,628 | \$ 1,378,913 | \$ 1,380,197 | \$ 1,381,481 | \$ 1,382,766 | \$ 1,384,050 | \$ 1,385,334 | \$ 1,386,618 |
| 90 | \$ 1,378,290 | \$ 1,379,575 | \$ 1,380,859 | \$ 1,382,143 | \$ 1,383,428 | \$ 1,384,712 | \$ 1,385,996 | \$ 1,387,281 | \$ 1,388,565 |
| 95 | \$ 1,380,237 | \$ 1,381,521 | \$ 1,382,805 | \$ 1,384,090 | \$ 1,385,374 | \$ 1,386,658 | \$ 1,387,943 | \$ 1,389,227 | \$ 1,390,511 |
| 100 | \$ 1,382,183 | \$ 1,383,468 | \$ 1,384,752 | \$ 1,386,036 | \$ 1,387,320 | \$ 1,388,605 | \$ 1,389,889 | \$ 1,391,173 | \$ 1,392,458 |

Table 6.4 provides total costs for the alternative based upon the above numbers. A spreadsheet, set up for this purpose, allows what-if scenarios, and changes in assumptions and unit costs. Cost items that may be potentially significant but are not included here (this monograph is meant to be illustrative only) include:

- Grading and compacting of pavement subgrade and
- Landscaping and finish work

Table 6.4.1 Case 5 - $\mathrm{Lj}=300 \mathrm{ft}$., $\mathrm{N}=1$ lane
a) Total Area to be Excavated in Square Yards (SY)

|  | Wength (ft) |  |  |  |  |  |  |  |  |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Width (ft) | $\mathbf{5 0}$ | $\mathbf{7 5}$ | $\mathbf{1 0 0}$ | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | $\mathbf{1 7 5}$ | $\mathbf{2 0 0}$ | $\mathbf{2 2 5}$ | $\mathbf{2 5 0}$ |
| $\mathbf{5 0}$ | 5,361 | 5,433 | 5,505 | 5,577 | 5,649 | 5,721 | 5,793 | 5,865 | 5,937 |
| $\mathbf{5 5}$ | 5,399 | 5,471 | 5,543 | 5,615 | 5,687 | 5,759 | 5,831 | 5,903 | 5,975 |
| $\mathbf{6 0}$ | 5,437 | 5,509 | 5,581 | 5,653 | 5,725 | 5,797 | 5,869 | 5,941 | 6,013 |
| $\mathbf{6 5}$ | 5,475 | 5,547 | 5,619 | 5,691 | 5,763 | 5,835 | 5,907 | 5,979 | 6,051 |
| $\mathbf{7 0}$ | 5,513 | 5,585 | 5,657 | 5,729 | 5,801 | 5,873 | 5,945 | 6,017 | 6,089 |
| $\mathbf{7 5}$ | 5,551 | 5,623 | 5,695 | 5,767 | 5,839 | 5,911 | 5,983 | 6,055 | 6,127 |
| $\mathbf{8 0}$ | 5,590 | 5,662 | 5,734 | 5,806 | 5,878 | 5,950 | 6,022 | 6,094 | 6,166 |
| $\mathbf{8 5}$ | 5,628 | 5,700 | 5,772 | 5,844 | 5,916 | 5,988 | 6,060 | 6,132 | 6,204 |
| $\mathbf{9 0}$ | 5,666 | 5,738 | 5,810 | 5,882 | 5,954 | 6,026 | 6,098 | 6,170 | 6,242 |
| $\mathbf{9 5}$ | 5,704 | 5,776 | 5,848 | 5,920 | 5,992 | 6,064 | 6,136 | 6,208 | 6,280 |
| $\mathbf{1 0 0}$ | 5,742 | 5,814 | 5,886 | 5,958 | 6,030 | 6,102 | 6,174 | 6,246 | 6,318 |

b) Areas to be Paved in Square Yards (SY)

| Width | Length (ft) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 50 | 75 | 100 | 125 | 150 | 175 | 200 | 225 | 250 |
| 50 | 4,115 | 4,142 | 4,170 | 4,197 | 4,225 | 4,252 | 4,280 | 4,308 | 4,335 |
| 55 | 4,115 | 4,142 | 4,170 | 4,197 | 4,225 | 4,252 | 4,280 | 4,308 | 4,335 |
| 60 | 4,115 | 4,142 | 4,170 | 4,197 | 4,225 | 4,252 | 4,280 | 4,308 | 4,335 |
| 65 | 4,115 | 4,142 | 4,170 | 4,197 | 4,225 | 4,252 | 4,280 | 4,308 | 4,335 |
| 70 | 4,115 | 4,142 | 4,170 | 4,197 | 4,225 | 4,252 | 4,280 | 4,308 | 4,335 |
| 75 | 4,115 | 4,142 | 4,170 | 4,197 | 4,225 | 4,252 | 4,280 | 4,308 | 4,335 |
| 80 | 4,115 | 4,142 | 4,170 | 4,197 | 4,225 | 4,252 | 4,280 | 4,308 | 4,335 |
| 85 | 4,115 | 4,142 | 4,170 | 4,197 | 4,225 | 4,252 | 4,280 | 4,308 | 4,335 |
| 90 | 4,115 | 4,142 | 4,170 | 4,197 | 4,225 | 4,252 | 4,280 | 4,308 | 4,335 |
| 95 | 4,115 | 4,142 | 4,170 | 4,197 | 4,225 | 4,252 | 4,280 | 4,308 | 4,335 |
| 100 | 4,115 | 4,142 | 4,170 | 4,197 | 4,225 | 4,252 | 4,280 | 4,308 | 4,335 |

## c) Total Costs for Alternative

| Width (ft) | Length (ft) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 50 |  | 75 |  | 100 |  | 125 |  | 150 |  | 175 |  | 200 |  | 225 |  | 250 |  |
| 50 | S | 179,607 | \$ | 180,892 | \$ | 182,176 | \$ | 183,460 | \$ | 184,745 | \$ | 186,029 | \$ | 187,313 | \$ | 188,598 | \$ | 189,882 |
| 55 | \$ | 179,702 | \$ | 180,987 | \$ | 182,271 | \$ | 183,555 | \$ | 184,840 | \$ | 186,124 | \$ | 187,408 | \$ | 188,693 | \$ | 189,977 |
| 60 | \$ | 179,798 | \$ | 181,082 | \$ | 182,366 | \$ | 183,651 | \$ | 184,935 | \$ | 186,219 | \$ | 187,504 | \$ | 188,788 | \$ | 190,072 |
| 65 | \$ | 179,893 | \$ | 181,177 | \$ | 182,461 | \$ | 183,746 | \$ | 185,030 | \$ | 186,314 | \$ | 187,599 | \$ | 188,883 | \$ | 190,167 |
| 70 | \$ | 179,988 | \$ | 181,272 | \$ | 182,556 | \$ | 183,841 | \$ | 185,125 | \$ | 186,409 | \$ | 187,694 | \$ | 188,978 | \$ | 190,262 |
| 75 | \$ | 180,083 | \$ | 181,367 | \$ | 182,652 | \$ | 183,936 | \$ | 185,220 | \$ | 186,505 | \$ | 187,789 | \$ | 189,073 | \$ | 190,358 |
| 80 | \$ | 180,178 | \$ | 181,462 | \$ | 182,747 | \$ | 184,031 | \$ | 185,315 | \$ | 186,600 | \$ | 187,884 | \$ | 189,168 | \$ | 190,453 |
| 85 | \$ | 180,273 | \$ | 181,558 | \$ | 182,842 | \$ | 184,126 | \$ | 185,411 | \$ | 186,695 | \$ | 187,979 | \$ | 189,264 | \$ | 190,548 |
| 90 | \$ | 180,368 | \$ | 181,653 | \$ | 182,937 | \$ | 184,221 | \$ | 185,506 | \$ | 186,790 | \$ | 188,074 | \$ | 189,359 | \$ | 190,643 |
| 95 | \$ | 180,464 | \$ | 181,748 | \$ | 183,032 | \$ | 184,316 | \$ | 185,601 | \$ | 186,885 | \$ | 188,169 | \$ | 189,454 | \$ | 190,738 |
| 100 | \$ | 180,559 | \$ | 181,843 | \$ | 183,127 | \$ | 184,412 | \$ | 185,696 | \$ | 186,980 | \$ | 188,265 | \$ | 189,549 | \$ | 190,833 |

Table 6.4.2 Case $\mathbf{5} \mathbf{- L j}=\mathbf{3 0 0} \mathrm{ft}$., $\mathrm{N}=2$ lanes
a) Total Area to be Excavated in Square Yards (SY)

|  | Width (ft) |  |  |  |  |  |  |  |  |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathbf{5 0}$ | $\mathbf{7 5}$ | $\mathbf{1 0 0}$ | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | $\mathbf{1 7 5}$ | $\mathbf{2 0 0}$ | $\mathbf{2 2 5}$ | $\mathbf{2 5 0}$ |
| $\mathbf{5 0}$ | 8,976 | 9,048 | 9,120 | 9,192 | 9,264 | 9,336 | 9,408 | 9,480 | 9,552 |
| $\mathbf{5 5}$ | 9,014 | 9,086 | 9,158 | 9,230 | 9,302 | 9,374 | 9,446 | 9,518 | 9,590 |
| $\mathbf{6 0}$ | 9,052 | 9,124 | 9,196 | 9,268 | 9,340 | 9,412 | 9,484 | 9,556 | 9,628 |
| $\mathbf{6 5}$ | 9,090 | 9,162 | 9,234 | 9,306 | 9,378 | 9,450 | 9,522 | 9,594 | 9,666 |
| $\mathbf{7 0}$ | 9,128 | 9,200 | 9,272 | 9,344 | 9,416 | 9,488 | 9,560 | 9,632 | 9,704 |
| $\mathbf{7 5}$ | 9,166 | 9,238 | 9,310 | 9,382 | 9,454 | 9,526 | 9,598 | 9,670 | 9,742 |
| $\mathbf{8 0}$ | 9,205 | 9,277 | 9,349 | 9,421 | 9,493 | 9,565 | 9,637 | 9,709 | 9,781 |
| $\mathbf{8 5}$ | 9,243 | 9,315 | 9,387 | 9,459 | 9,531 | 9,603 | 9,675 | 9,747 | 9,819 |
| $\mathbf{9 0}$ | 9,281 | 9,353 | 9,425 | 9,497 | 9,569 | 9,641 | 9,713 | 9,785 | 9,857 |
| $\mathbf{9 5}$ | 9,319 | 9,391 | 9,463 | 9,535 | 9,607 | 9,679 | 9,751 | 9,823 | 9,895 |
| $\mathbf{1 0 0}$ | 9,357 | 9,429 | 9,501 | 9,573 | 9,645 | 9,717 | 9,789 | 9,861 | 9,933 |

b) Areas to be Paved in Square Yards (SY)

| Width | $\mathbf{5 0}$ | $\mathbf{7 5}$ | $\mathbf{1 0 0}$ | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | $\mathbf{1 7 5}$ | $\mathbf{2 0 0}$ | $\mathbf{2 2 5}$ | $\mathbf{2 5 0}$ |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathbf{5 0}$ | 7,730 | 7,757 | 7,785 | 7,812 | 7,840 | 7,867 | 7,895 | 7,923 |
|  | 7,730 | 7,757 | 7,785 | 7,812 | 7,840 | 7,867 | 7,895 | 7,923 | 7,950 |
| $\mathbf{6 0}$ | 7,730 | 7,757 | 7,785 | 7,812 | 7,840 | 7,867 | 7,895 | 7,923 | 7,950 |
| $\mathbf{6 5}$ | 7,730 | 7,757 | 7,785 | 7,812 | 7,840 | 7,867 | 7,895 | 7,923 | 7,950 |
| $\mathbf{7 0}$ | 7,730 | 7,757 | 7,785 | 7,812 | 7,840 | 7,867 | 7,895 | 7,923 | 7,950 |
| $\mathbf{7 5}$ | 7,730 | 7,757 | 7,785 | 7,812 | 7,840 | 7,867 | 7,895 | 7,923 | 7,950 |
| $\mathbf{8 0}$ | 7,730 | 7,757 | 7,785 | 7,812 | 7,840 | 7,867 | 7,895 | 7,923 | 7,950 |
| $\mathbf{8 5}$ | 7,730 | 7,757 | 7,785 | 7,812 | 7,840 | 7,867 | 7,895 | 7,923 | 7,950 |
| $\mathbf{9 0}$ | 7,730 | 7,757 | 7,785 | 7,812 | 7,840 | 7,867 | 7,895 | 7,923 | 7,950 |
| $\mathbf{9 5}$ | 7,730 | 7,757 | 7,785 | 7,812 | 7,840 | 7,867 | 7,895 | 7,923 | 7,950 |
| $\mathbf{1 0 0}$ | 7,730 | 7,757 | 7,785 | 7,812 | 7,840 | 7,867 | 7,895 | 7,923 | 7,950 |

## c) Total Costs for Alternative

| Width (ft) | Length (ft) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 50 |  | 75 |  | 100 |  | 125 |  | 150 |  | 175 |  | 200 |  | 225 |  | 250 |
| 50 | \$ 327,780 | \$ | 329,064 | \$ | 330,349 | \$ | 331,633 | \$ | 332,917 | \$ | 334,202 | \$ | 335,486 | \$ | 336,770 | \$ | 338,055 |
| 55 | \$ 327,875 | \$ | 329,160 | \$ | 330,444 | \$ | 331,728 | \$ | 333,012 | \$ | 334,297 | \$ | 335,581 | \$ | 336,865 | \$ | 338,150 |
| 60 | \$ 327,970 | \$ | 329,255 | \$ | 330,539 | \$ | 331,823 | \$ | 333,108 | \$ | 334,392 | \$ | 335,676 | \$ | 336,961 | \$ | 338,245 |
| 65 | \$ 328,065 | \$ | 329,350 | \$ | 330,634 | \$ | 331,918 | \$ | 333,203 | \$ | 334,487 | \$ | 335,771 | \$ | 337,056 | \$ | 338,340 |
| 70 | \$ 328,161 | \$ | 329,445 | \$ | 330,729 | \$ | 332,014 | \$ | 333,298 | \$ | 334,582 | \$ | 335,867 | \$ | 337,151 | \$ | 338,435 |
| 75 | \$ 328,256 | \$ | 329,540 | \$ | 330,824 | \$ | 332,109 | \$ | 333,393 | \$ | 334,677 | \$ | 335,962 | \$ | 337,246 | \$ | 338,530 |
| 80 | \$ 328,351 | \$ | 329,635 | \$ | 330,919 | \$ | 332,204 | \$ | 333,488 | \$ | 334,772 | \$ | 336,057 | \$ | 337,341 | \$ | 338,625 |
| 85 | \$ 328,446 | \$ | 329,730 | \$ | 331,015 | \$ | 332,299 | \$ | 333,583 | \$ | 334,868 | \$ | 336,152 | \$ | 337,436 | \$ | 338,721 |
| 90 | \$ 328,541 | \$ | 329,825 | \$ | 331,110 | \$ | 332,394 | \$ | 333,678 | \$ | 334,963 | \$ | 336,247 | \$ | 337,531 | \$ | 338,816 |
| 95 | \$ 328,636 | \$ | 329,921 | \$ | 331,205 | \$ | 332,489 | \$ | 333,774 | \$ | 335,058 | \$ | 336,342 | \$ | 337,627 | \$ | 338,911 |
| 100 | \$ 328,731 | \$ | 330,016 | \$ | 331,300 | \$ | 332,584 | \$ | 333,869 | \$ | 335,153 | \$ | 336,437 | \$ | 337,722 | \$ | 339,006 |

Table 6.4.3 Case 5 - $\mathrm{Lj}=350 \mathrm{ft}$., $\mathrm{N}=1$ lane
a) Total Area to be Excavated in Square Yards (SY)

|  | Width (ft) |  |  |  |  |  |  |  |  |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathbf{5 0}$ | $\mathbf{7 5}$ | $\mathbf{1 0 0}$ | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | $\mathbf{1 7 5}$ | $\mathbf{2 0 0}$ | $\mathbf{2 2 5}$ | $\mathbf{2 5 0}$ |
| $\mathbf{5 0}$ | 5,961 | 6,033 | 6,105 | 6,177 | 6,249 | 6,321 | 6,393 | 6,465 | 6,537 |
| $\mathbf{5 5}$ | 5,999 | 6,071 | 6,143 | 6,215 | 6,287 | 6,359 | 6,431 | 6,503 | 6,575 |
| $\mathbf{6 0}$ | 6,037 | 6,109 | 6,181 | 6,253 | 6,325 | 6,397 | 6,469 | 6,541 | 6,613 |
| $\mathbf{6 5}$ | 6,075 | 6,147 | 6,219 | 6,291 | 6,363 | 6,435 | 6,507 | 6,579 | 6,651 |
| $\mathbf{7 0}$ | 6,113 | 6,185 | 6,257 | 6,329 | 6,401 | 6,473 | 6,545 | 6,617 | 6,689 |
| $\mathbf{7 5}$ | 6,151 | 6,223 | 6,295 | 6,367 | 6,439 | 6,511 | 6,583 | 6,655 | 6,727 |
| $\mathbf{8 0}$ | 6,190 | 6,262 | 6,334 | 6,406 | 6,478 | 6,550 | 6,622 | 6,694 | 6,766 |
| $\mathbf{8 5}$ | 6,228 | 6,300 | 6,372 | 6,444 | 6,516 | 6,588 | 6,660 | 6,732 | 6,804 |
| $\mathbf{9 0}$ | 6,266 | 6,338 | 6,410 | 6,482 | 6,554 | 6,626 | 6,698 | 6,770 | 6,842 |
| $\mathbf{9 5}$ | 6,304 | 6,376 | 6,448 | 6,520 | 6,592 | 6,664 | 6,736 | 6,808 | 6,880 |
| $\mathbf{1 0 0}$ | 6,342 | 6,414 | 6,486 | 6,558 | 6,630 | 6,702 | 6,774 | 6,846 | 6,918 |

b) Areas to be Paved in Square Yards (SY)

| Width | Length (ft) |  |  |  |  |  |  |  |  |  |  |  | $\mathbf{5 0}$ | $\mathbf{7 5}$ | $\mathbf{1 0 0}$ | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | $\mathbf{1 7 5}$ | $\mathbf{2 0 0}$ | $\mathbf{2 2 5}$ | $\mathbf{2 5 0}$ |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4,715 | 4,742 | 4,770 | 4,797 | 4,825 | 4,852 | 4,880 | 4,908 | 4,935 |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 4,715 | 4,742 | 4,770 | 4,797 | 4,825 | 4,852 | 4,880 | 4,908 | 4,935 |  |  |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{6 0}$ | 4,715 | 4,742 | 4,770 | 4,797 | 4,825 | 4,852 | 4,880 | 4,908 | 4,935 |  |  |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{6 5}$ | 4,715 | 4,742 | 4,770 | 4,797 | 4,825 | 4,852 | 4,880 | 4,908 | 4,935 |  |  |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{7 0}$ | 4,715 | 4,742 | 4,770 | 4,797 | 4,825 | 4,852 | 4,880 | 4,908 | 4,935 |  |  |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{7 5}$ | 4,715 | 4,742 | 4,770 | 4,797 | 4,825 | 4,852 | 4,880 | 4,908 | 4,935 |  |  |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{8 0}$ | 4,715 | 4,742 | 4,770 | 4,797 | 4,825 | 4,852 | 4,880 | 4,908 | 4,935 |  |  |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{8 5}$ | 4,715 | 4,742 | 4,770 | 4,797 | 4,825 | 4,852 | 4,880 | 4,908 | 4,935 |  |  |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{9 0}$ | 4,715 | 4,742 | 4,770 | 4,797 | 4,825 | 4,852 | 4,880 | 4,908 | 4,935 |  |  |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{9 5}$ | 4,715 | 4,742 | 4,770 | 4,797 | 4,825 | 4,852 | 4,880 | 4,908 | 4,935 |  |  |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{1 0 0}$ | 4,715 | 4,742 | 4,770 | 4,797 | 4,825 | 4,852 | 4,880 | 4,908 | 4,935 |  |  |  |  |  |  |  |  |  |  |  |  |

## c) Total Costs for Alternative

| Width (ft) | Length (ft) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 50 |  | 75 |  | 100 |  | 125 |  | 150 |  | 175 |  | 200 |  | 225 |  | 250 |  |
| 50 | \$ | 204,200 | \$ | 205,485 | \$ | 206,769 | \$ | 208,053 | \$ | 209,338 | \$ | 210,622 | \$ | 211,906 | \$ | 213,191 | \$ | 214,475 |
| 55 | \$ | 204,295 | \$ | 205,580 | \$ | 206,864 | \$ | 208,148 | \$ | 209,433 | \$ | 210,717 | \$ | 212,001 | \$ | 213,286 | \$ | 214,570 |
| 60 | \$ | 204,391 | \$ | 205,675 | \$ | 206,959 | \$ | 208,244 | \$ | 209,528 | \$ | 210,812 | \$ | 212,097 | \$ | 213,381 | \$ | 214,665 |
| 65 | \$ | 204,486 | \$ | 205,770 | \$ | 207,054 | \$ | 208,339 | \$ | 209,623 | \$ | 210,907 | \$ | 212,192 | \$ | 213,476 | \$ | 214,760 |
| 70 | \$ | 204,581 | \$ | 205,865 | \$ | 207,149 | \$ | 208,434 | \$ | 209,718 | \$ | 211,002 | \$ | 212,287 | \$ | 213,571 | \$ | 214,855 |
| 75 | \$ | 204,676 | \$ | 205,960 | \$ | 207,245 | \$ | 208,529 | \$ | 209,813 | \$ | 211,098 | \$ | 212,382 | \$ | 213,666 | \$ | 214,951 |
| 80 | \$ | 204,771 | \$ | 206,055 | \$ | 207,340 | \$ | 208,624 | \$ | 209,908 | \$ | 211,193 | \$ | 212,477 | \$ | 213,761 | \$ | 215,046 |
| 85 | \$ | 204,866 | \$ | 206,151 | \$ | 207,435 | \$ | 208,719 | \$ | 210,004 | \$ | 211,288 | \$ | 212,572 | \$ | 213,856 | \$ | 215,141 |
| 90 | \$ | 204,961 | \$ | 206,246 | \$ | 207,530 | \$ | 208,814 | \$ | 210,099 | \$ | 211,383 | \$ | 212,667 | \$ | 213,952 | \$ | 215,236 |
| 95 | \$ | 205,056 | \$ | 206,341 | \$ | 207,625 | \$ | 208,909 | \$ | 210,194 | \$ | 211,478 | \$ | 212,762 | \$ | 214,047 | \$ | 215,331 |
| 100 | \$ | 205,152 | \$ | 206,436 | \$ | 207,720 | \$ | 209,005 | \$ | 210,289 | \$ | 211,573 | \$ | 212,858 | \$ | 214,142 | \$ | 215,426 |

Table 6.4.4 Case $\mathbf{5}-\mathbf{L j}=\mathbf{3 5 0} \mathrm{ft} ., \mathrm{N}=2$ lanes
a) Total Area to be Excavated in Square Yards (SY)

|  | Length (ft) |  |  |  |  |  |  |  |  |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Width (ft) | $\mathbf{5 0}$ | $\mathbf{7 5}$ | $\mathbf{1 0 0}$ | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | $\mathbf{1 7 5}$ | $\mathbf{2 0 0}$ | $\mathbf{2 2 5}$ | $\mathbf{2 5 0}$ |
| $\mathbf{5 0}$ | 10,176 | 10,248 | 10,320 | 10,392 | 10,464 | 10,536 | 10,608 | 10,680 | 10,752 |
| $\mathbf{5 5}$ | 10,214 | 10,286 | 10,358 | 10,430 | 10,502 | 10,574 | 10,646 | 10,718 | 10,790 |
| $\mathbf{6 0}$ | 10,252 | 10,324 | 10,396 | 10,468 | 10,540 | 10,612 | 10,684 | 10,756 | 10,828 |
| $\mathbf{6 5}$ | 10,290 | 10,362 | 10,434 | 10,506 | 10,578 | 10,650 | 10,722 | 10,794 | 10,866 |
| $\mathbf{7 0}$ | 10,328 | 10,400 | 10,472 | 10,544 | 10,616 | 10,688 | 10,760 | 10,832 | 10,904 |
| $\mathbf{7 5}$ | 10,366 | 10,438 | 10,510 | 10,582 | 10,654 | 10,726 | 10,798 | 10,870 | 10,942 |
| $\mathbf{8 0}$ | 10,405 | 10,477 | 10,549 | 10,621 | 10,693 | 10,765 | 10,837 | 10,909 | 10,981 |
| $\mathbf{8 5}$ | 10,443 | 10,515 | 10,587 | 10,659 | 10,731 | 10,803 | 10,875 | 10,947 | 11,019 |
| $\mathbf{9 0}$ | 10,481 | 10,553 | 10,625 | 10,697 | 10,769 | 10,841 | 10,913 | 10,985 | 11,057 |
| $\mathbf{9 5}$ | 10,519 | 10,591 | 10,663 | 10,735 | 10,807 | 10,879 | 10,951 | 11,023 | 11,095 |
| $\mathbf{1 0 0}$ | 10,557 | 10,629 | 10,701 | 10,773 | 10,845 | 10,917 | 10,989 | 11,061 | 11,133 |

b) Areas to be Paved in Square Yards (SY)

| Width | Length (ft) |  |  |  |  |  |  |  |  |  |  | $\mathbf{5 0}$ | $\mathbf{7 5}$ | $\mathbf{1 0 0}$ | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | $\mathbf{1 7 5}$ | $\mathbf{2 0 0}$ | $\mathbf{2 2 5}$ | $\mathbf{2 5 0}$ |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 8,930 | 8,957 | 8,985 | 9,012 | 9,040 | 9,067 | 9,095 | 9,123 | 9,150 |  |  |  |  |  |  |  |  |  |  |  |
|  | 8,930 | 8,957 | 8,985 | 9,012 | 9,040 | 9,067 | 9,095 | 9,123 | 9,150 |  |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{6 0}$ | 8,930 | 8,957 | 8,985 | 9,012 | 9,040 | 9,067 | 9,095 | 9,123 | 9,150 |  |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{6 5}$ | 8,930 | 8,957 | 8,985 | 9,012 | 9,040 | 9,067 | 9,095 | 9,123 | 9,150 |  |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{7 0}$ | 8,930 | 8,957 | 8,985 | 9,012 | 9,040 | 9,067 | 9,095 | 9,123 | 9,150 |  |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{7 5}$ | 8,930 | 8,957 | 8,985 | 9,012 | 9,040 | 9,067 | 9,095 | 9,123 | 9,150 |  |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{8 0}$ | 8,930 | 8,957 | 8,985 | 9,012 | 9,040 | 9,067 | 9,095 | 9,123 | 9,150 |  |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{8 5}$ | 8,930 | 8,957 | 8,985 | 9,012 | 9,040 | 9,067 | 9,095 | 9,123 | 9,150 |  |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{9 0}$ | 8,930 | 8,957 | 8,985 | 9,012 | 9,040 | 9,067 | 9,095 | 9,123 | 9,150 |  |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{9 5}$ | 8,930 | 8,957 | 8,985 | 9,012 | 9,040 | 9,067 | 9,095 | 9,123 | 9,150 |  |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{1 0 0}$ | 8,930 | 8,957 | 8,985 | 9,012 | 9,040 | 9,067 | 9,095 | 9,123 | 9,150 |  |  |  |  |  |  |  |  |  |  |  |

## c) Total Costs for Alternative

| Width (ft) | Length (ft) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 50 |  | 75 |  | 100 |  | 125 |  | 150 |  | 175 |  | 200 |  | 225 |  | 250 |
| 50 | \$ | 376,966 | \$ | 378,250 | \$ | 379,535 | \$ | 380,819 | \$ | 382,103 | \$ | 383,388 | \$ | 384,672 | \$ | 385,956 | \$ | 387,241 |
| 55 | \$ | 377,061 | \$ | 378,345 | \$ | 379,630 | \$ | 380,914 | \$ | 382,198 | \$ | 383,483 | \$ | 384,767 | \$ | 386,051 | \$ | 387,336 |
| 60 | \$ | 377,156 | \$ | 378,441 | \$ | 379,725 | \$ | 381,009 | \$ | 382,294 | \$ | 383,578 | \$ | 384,862 | \$ | 386,147 | \$ | 387,431 |
| 65 | \$ | 377,251 | \$ | 378,536 | \$ | 379,820 | \$ | 381,104 | \$ | 382,389 | \$ | 383,673 | \$ | 384,957 | \$ | 386,242 | \$ | 387,526 |
| 70 | \$ | 377,347 | \$ | 378,631 | \$ | 379,915 | \$ | 381,200 | \$ | 382,484 | \$ | 383,768 | \$ | 385,052 | \$ | 386,337 | \$ | 387,621 |
| 75 | \$ | 377,442 | \$ | 378,726 | \$ | 380,010 | \$ | 381,295 | \$ | 382,579 | \$ | 383,863 | \$ | 385,148 | \$ | 386,432 | \$ | 387,716 |
| 80 | \$ | 377,537 | \$ | 378,821 | \$ | 380,105 | \$ | 381,390 | \$ | 382,674 | \$ | 383,958 | \$ | 385,243 | \$ | 386,527 | \$ | 387,811 |
| 85 | \$ | 377,632 | \$ | 378,916 | \$ | 380,201 | \$ | 381,485 | \$ | 382,769 | \$ | 384,054 | \$ | 385,338 | \$ | 386,622 | \$ | 387,907 |
| 90 | \$ | 377,727 | \$ | 379,011 | \$ | 380,296 | \$ | 381,580 | \$ | 382,864 | \$ | 384,149 | \$ | 385,433 | \$ | 386,717 | \$ | 388,002 |
| 95 | \$ | 377,822 | \$ | 379,107 | \$ | 380,391 | \$ | 381,675 | \$ | 382,960 | \$ | 384,244 | \$ | 385,528 | \$ | 386,812 | \$ | 388,097 |
| 100 | \$ | 377,917 | \$ | 379,202 | \$ | 380,486 | \$ | 381,770 | \$ | 383,055 | \$ | 384,339 | \$ | 385,623 | \$ | 386,908 | \$ | 388,192 |

Table 6.4.5 Case $5-\mathrm{Lj}=400 \mathrm{ft}$., $\mathrm{N}=1$ lane
a) Total Area to be Excavated in Square Yards (SY)

|  | Length (ft) |  |  |  |  |  |  |  |  |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Width (ft) | $\mathbf{5 0}$ | $\mathbf{7 5}$ | $\mathbf{1 0 0}$ | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | $\mathbf{1 7 5}$ | $\mathbf{2 0 0}$ | $\mathbf{2 2 5}$ | $\mathbf{2 5 0}$ |
| $\mathbf{5 0}$ | 6,561 | 6,633 | 6,705 | 6,777 | 6,849 | 6,921 | 6,993 | 7,065 | 7,137 |
| $\mathbf{5 5}$ | 6,599 | 6,671 | 6,743 | 6,815 | 6,887 | 6,959 | 7,031 | 7,103 | 7,175 |
| $\mathbf{6 0}$ | 6,637 | 6,709 | 6,781 | 6,853 | 6,925 | 6,997 | 7,069 | 7,141 | 7,213 |
| $\mathbf{6 5}$ | 6,675 | 6,747 | 6,819 | 6,891 | 6,963 | 7,035 | 7,107 | 7,179 | 7,251 |
| $\mathbf{7 0}$ | 6,713 | 6,785 | 6,857 | 6,929 | 7,001 | 7,073 | 7,145 | 7,217 | 7,289 |
| $\mathbf{7 5}$ | 6,751 | 6,823 | 6,895 | 6,967 | 7,039 | 7,111 | 7,183 | 7,255 | 7,327 |
| $\mathbf{8 0}$ | 6,790 | 6,862 | 6,934 | 7,006 | 7,078 | 7,150 | 7,222 | 7,294 | 7,366 |
| $\mathbf{8 5}$ | 6,828 | 6,900 | 6,972 | 7,044 | 7,116 | 7,188 | 7,260 | 7,332 | 7,404 |
| $\mathbf{9 0}$ | 6,866 | 6,938 | 7,010 | 7,082 | 7,154 | 7,226 | 7,298 | 7,370 | 7,442 |
| $\mathbf{9 5}$ | 6,904 | 6,976 | 7,048 | 7,120 | 7,192 | 7,264 | 7,336 | 7,408 | 7,480 |
| $\mathbf{1 0 0}$ | 6,942 | 7,014 | 7,086 | 7,158 | 7,230 | 7,302 | 7,374 | 7,446 | 7,518 |

b) Areas to be Paved in Square Yards (SY)

| Width | Length (ft) |  |  |  |  |  |  |  |  |  |  | $\mathbf{5 0}$ | $\mathbf{7 5}$ | $\mathbf{1 0 0}$ | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | $\mathbf{1 7 5}$ | $\mathbf{2 0 0}$ | $\mathbf{2 2 5}$ | $\mathbf{2 5 0}$ |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 5,315 | 5,342 | 5,370 | 5,397 | 5,425 | 5,452 | 5,480 | 5,508 | 5,535 |  |  |  |  |  |  |  |  |  |  |  |
|  | 5,315 | 5,342 | 5,370 | 5,397 | 5,425 | 5,452 | 5,480 | 5,508 | 5,535 |  |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{6 0}$ | 5,315 | 5,342 | 5,370 | 5,397 | 5,425 | 5,452 | 5,480 | 5,508 | 5,535 |  |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{6 5}$ | 5,315 | 5,342 | 5,370 | 5,397 | 5,425 | 5,452 | 5,480 | 5,508 | 5,535 |  |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{7 0}$ | 5,315 | 5,342 | 5,370 | 5,397 | 5,425 | 5,452 | 5,480 | 5,508 | 5,535 |  |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{7 5}$ | 5,315 | 5,342 | 5,370 | 5,397 | 5,425 | 5,452 | 5,480 | 5,508 | 5,535 |  |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{8 0}$ | 5,315 | 5,342 | 5,370 | 5,397 | 5,425 | 5,452 | 5,480 | 5,508 | 5,535 |  |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{8 5}$ | 5,315 | 5,342 | 5,370 | 5,397 | 5,425 | 5,452 | 5,480 | 5,508 | 5,535 |  |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{9 0}$ | 5,315 | 5,342 | 5,370 | 5,397 | 5,425 | 5,452 | 5,480 | 5,508 | 5,535 |  |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{9 5}$ | 5,315 | 5,342 | 5,370 | 5,397 | 5,425 | 5,452 | 5,480 | 5,508 | 5,535 |  |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{1 0 0}$ | 5,315 | 5,342 | 5,370 | 5,397 | 5,425 | 5,452 | 5,480 | 5,508 | 5,535 |  |  |  |  |  |  |  |  |  |  |  |

## c) Total Costs for Alternative

| Width (ft) | Length (ft) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 50 |  | 75 |  | 100 |  | 125 |  | 150 |  | 175 |  | 200 |  | 225 |  | 250 |
| 50 | \$ | 228,793 | \$ | 230,078 | \$ | 231,362 | \$ | 232,646 | \$ | 233,931 | \$ | 235,215 | \$ | 236,499 | \$ | 237,784 | \$ | 239,068 |
| 55 | \$ | 228,888 | \$ | 230,173 | \$ | 231,457 | \$ | 232,741 | \$ | 234,026 | \$ | 235,310 | \$ | 236,594 | \$ | 237,879 | \$ | 239,163 |
| 60 | \$ | 228,984 | \$ | 230,268 | \$ | 231,552 | \$ | 232,837 | \$ | 234,121 | \$ | 235,405 | \$ | 236,689 | \$ | 237,974 | \$ | 239,258 |
| 65 | \$ | 229,079 | \$ | 230,363 | \$ | 231,647 | \$ | 232,932 | \$ | 234,216 | \$ | 235,500 | \$ | 236,785 | \$ | 238,069 | \$ | 239,353 |
| 70 | \$ | 229,174 | \$ | 230,458 | \$ | 231,742 | \$ | 233,027 | \$ | 234,311 | \$ | 235,595 | \$ | 236,880 | \$ | 238,164 | \$ | 239,448 |
| 75 | \$ | 229,269 | \$ | 230,553 | \$ | 231,838 | \$ | 233,122 | \$ | 234,406 | \$ | 235,691 | \$ | 236,975 | \$ | 238,259 | \$ | 239,544 |
| 80 | \$ | 229,364 | \$ | 230,648 | \$ | 231,933 | \$ | 233,217 | \$ | 234,501 | \$ | 235,786 | \$ | 237,070 | \$ | 238,354 | \$ | 239,639 |
| 85 | \$ | 229,459 | \$ | 230,744 | \$ | 232,028 | \$ | 233,312 | \$ | 234,597 | \$ | 235,881 | \$ | 237,165 | \$ | 238,449 | \$ | 239,734 |
| 90 | \$ | 229,554 | \$ | 230,839 | \$ | 232,123 | \$ | 233,407 | \$ | 234,692 | \$ | 235,976 | \$ | 237,260 | \$ | 238,545 | \$ | 239,829 |
| 95 | \$ | 229,649 | \$ | 230,934 | \$ | 232,218 | \$ | 233,502 | \$ | 234,787 | \$ | 236,071 | \$ | 237,355 | \$ | 238,640 | \$ | 239,924 |
| 100 | \$ | 229,745 | \$ | 231,029 | \$ | 232,313 | \$ | 233,598 | \$ | 234,882 | \$ | 236,166 | \$ | 237,451 | \$ | 238,735 | \$ | 240,019 |

Table 6.4.6 Case $\mathbf{5}-\mathbf{L j}=400 \mathrm{ft}$., $\mathrm{N}=2$ lanes
a) Total Area to be Excavated in Square Yards (SY)

|  | Width (ft) |  |  |  |  |  |  |  |  |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathbf{5 0}$ | $\mathbf{7 5}$ | $\mathbf{1 0 0}$ | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | $\mathbf{1 7 5}$ | $\mathbf{2 0 0}$ | $\mathbf{2 2 5}$ | $\mathbf{2 5 0}$ |
| $\mathbf{5 0}$ | 11,376 | 11,448 | 11,520 | 11,592 | 11,664 | 11,736 | 11,808 | 11,880 | 11,952 |
| $\mathbf{5 5}$ | 11,414 | 11,486 | 11,558 | 11,630 | 11,702 | 11,774 | 11,846 | 11,918 | 11,990 |
| $\mathbf{6 0}$ | 11,452 | 11,524 | 11,596 | 11,668 | 11,740 | 11,812 | 11,884 | 11,956 | 12,028 |
| $\mathbf{6 5}$ | 11,490 | 11,562 | 11,634 | 11,706 | 11,778 | 11,850 | 11,922 | 11,994 | 12,066 |
| $\mathbf{7 0}$ | 11,528 | 11,600 | 11,672 | 11,744 | 11,816 | 11,888 | 11,960 | 12,032 | 12,104 |
| $\mathbf{7 5}$ | 11,566 | 11,638 | 11,710 | 11,782 | 11,854 | 11,926 | 11,998 | 12,070 | 12,142 |
| $\mathbf{8 0}$ | 11,605 | 11,677 | 11,749 | 11,821 | 11,893 | 11,965 | 12,037 | 12,109 | 12,181 |
| $\mathbf{8 5}$ | 11,643 | 11,715 | 11,787 | 11,859 | 11,931 | 12,003 | 12,075 | 12,147 | 12,219 |
| $\mathbf{9 0}$ | 11,681 | 11,753 | 11,825 | 11,897 | 11,969 | 12,041 | 12,113 | 12,185 | 12,257 |
| $\mathbf{9 5}$ | 11,719 | 11,791 | 11,863 | 11,935 | 12,007 | 12,079 | 12,151 | 12,223 | 12,295 |
| $\mathbf{1 0 0}$ | 11,757 | 11,829 | 11,901 | 11,973 | 12,045 | 12,117 | 12,189 | 12,261 | 12,333 |

b) Areas to be Paved in Square Yards (SY)

| Width | $\mathbf{5 0}$ | $\mathbf{7 5}$ | $\mathbf{1 0 0}$ | $\mathbf{1 2 5}$ | $\mathbf{1 5 0}$ | $\mathbf{1 7 5}$ | $\mathbf{2 0 0}$ | $\mathbf{2 2 5}$ | $\mathbf{2 5 0}$ |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathbf{5 0}$ | 10,130 | 10,157 | 10,185 | 10,212 | 10,240 | 10,267 | 10,295 | 10,323 |
|  | 10,130 | 10,157 | 10,185 | 10,212 | 10,240 | 10,267 | 10,295 | 10,323 | 10,350 |
| $\mathbf{6 0}$ | 10,130 | 10,157 | 10,185 | 10,212 | 10,240 | 10,267 | 10,295 | 10,323 | 10,350 |
| $\mathbf{6 5}$ | 10,130 | 10,157 | 10,185 | 10,212 | 10,240 | 10,267 | 10,295 | 10,323 | 10,350 |
| $\mathbf{7 0}$ | 10,130 | 10,157 | 10,185 | 10,212 | 10,240 | 10,267 | 10,295 | 10,323 | 10,350 |
| $\mathbf{7 5}$ | 10,130 | 10,157 | 10,185 | 10,212 | 10,240 | 10,267 | 10,295 | 10,323 | 10,350 |
| $\mathbf{8 0}$ | 10,130 | 10,157 | 10,185 | 10,212 | 10,240 | 10,267 | 10,295 | 10,323 | 10,350 |
| $\mathbf{8 5}$ | 10,130 | 10,157 | 10,185 | 10,212 | 10,240 | 10,267 | 10,295 | 10,323 | 10,350 |
| $\mathbf{9 0}$ | 10,130 | 10,157 | 10,185 | 10,212 | 10,240 | 10,267 | 10,295 | 10,323 | 10,350 |
| $\mathbf{9 5}$ | 10,130 | 10,157 | 10,185 | 10,212 | 10,240 | 10,267 | 10,295 | 10,323 | 10,350 |
| $\mathbf{1 0 0}$ | 10,130 | 10,157 | 10,185 | 10,212 | 10,240 | 10,267 | 10,295 | 10,323 | 10,350 |

## c) Total Costs for Alternative

| Width (ft) | Length (ft) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 50 |  | 75 |  | 100 |  | 125 |  | 150 |  | 175 |  | 200 |  | 225 |  | 250 |
| 50 | \$ | 426,152 | \$ | 427,436 | \$ | 428,721 | \$ | 430,005 | \$ | 431,289 | \$ | 432,574 | \$ | 433,858 | \$ | 435,142 | \$ | 436,427 |
| 55 | \$ | 426,247 | \$ | 427,531 | \$ | 428,816 | \$ | 430,100 | \$ | 431,384 | \$ | 432,669 | \$ | 433,953 | \$ | 435,237 | \$ | 436,522 |
| 60 | \$ | 426,342 | \$ | 427,627 | \$ | 428,911 | \$ | 430,195 | \$ | 431,480 | \$ | 432,764 | \$ | 434,048 | \$ | 435,333 | \$ | 436,617 |
| 65 | \$ | 426,437 | \$ | 427,722 | \$ | 429,006 | \$ | 430,290 | \$ | 431,575 | \$ | 432,859 | \$ | 434,143 | \$ | 435,428 | \$ | 436,712 |
| 70 | \$ | 426,533 | \$ | 427,817 | \$ | 429,101 | \$ | 430,385 | \$ | 431,670 | \$ | 432,954 | \$ | 434,238 | \$ | 435,523 | \$ | 436,807 |
| 75 | \$ | 426,628 | \$ | 427,912 | \$ | 429,196 | \$ | 430,481 | \$ | 431,765 | \$ | 433,049 | \$ | 434,334 | \$ | 435,618 | \$ | 436,902 |
| 80 | \$ | 426,723 | \$ | 428,007 | \$ | 429,291 | \$ | 430,576 | \$ | 431,860 | \$ | 433,144 | \$ | 434,429 | \$ | 435,713 | \$ | 436,997 |
| 85 | \$ | 426,818 | \$ | 428,102 | \$ | 429,387 | \$ | 430,671 | \$ | 431,955 | \$ | 433,240 | \$ | 434,524 | \$ | 435,808 | \$ | 437,093 |
| 90 | \$ | 426,913 | \$ | 428,197 | \$ | 429,482 | \$ | 430,766 | \$ | 432,050 | \$ | 433,335 | \$ | 434,619 | \$ | 435,903 | \$ | 437,188 |
| 95 | \$ | 427,008 | \$ | 428,293 | \$ | 429,577 | \$ | 430,861 | \$ | 432,145 | \$ | 433,430 | \$ | 434,714 | \$ | 435,998 | \$ | 437,283 |
| 100 | \$ | 427,103 | \$ | 428,388 | \$ | 429,672 | \$ | 430,956 | \$ | 432,241 | \$ | 433,525 | \$ | 434,809 | \$ | 436,094 | \$ | 437,378 |

## EVALUATION OF ALTERNATIVES

As indicated previously there exist several approaches to evaluating which are the best alternatives. For example, one might examine the cost effectiveness of each alternative design with respect to each of the operational outputs. Figure 6.1 illustrates the concept. Case 4's cost is significantly lower than the other two alternative costs yet its percent reduction in delay is only minimally lower (part a) and its increase in fuel consumption is actually lower as well (part b). This is known as the "cost effectiveness" approach to evaluating alternatives. One of its main advantages is that it eliminates the heavy reliance on numbers and scores that other approaches use in an attempt to combine different measures.


Figure 6.1 Cost Effectiveness Example

## REFERENCES

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3. Highway Capacity Manual, Special Report 209 - Third Edition, Transportation Research Board, National Research Council, Washington, D.C., 1998.
4. Harwood, D. and W. Glauz, NCHRP Synthesis of Highway Practice 281: Operational Impacts of Median Width on Larger Vehicles, Transportation Research Board, National Research Council, Washington, D.C., 2000.
5. Harwood, D., M. Pietrucha, M. Wooldridge, R. Brydia, and K. Fitzpatrick, NCHRP Report 375: Median Intersection Design, Transportation Research Board, National Research Council, Washington, D.C., 1995.
6. Federal Highway Administration, Manual on Uniform Traffic Control Devices for Streets and Highways, U.S. Department of Transportation, Washington, D.C., 1988.
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10. McShane, W.R., R. P. Roess, E. S. Prassas. Traffic Engineering, 2nd Ed., Prentice-Hall, Inc., 1998.
11. Elefteriadou, L., J.D. Leonard II, G. List, H. Lieu, M. Thomas, R. Giguere, G. Johnson, R. Brewish. "Beyond the Highway Capacity Manual: Framework for Selecting Simulation Models in Traffic Operational Analysis," Transportation Research Record 1678, Transportation Research Record, 1999.

## APPENDIX 1: ANNOTATED BIBLIOGRAPHY

The most basic references for highway design and operation references are already familiar to most readers of this report. These include AASHTO's A Policy on Geometric Design of Highways and Streets (1994), the Manual on Uniform Traffic Control Devices (1988), and the Highway Capacity Manual (1998). This report has also made extensive use of the Highway Capacity Software (Release 3, 1999) and NETSIM, a simulation program within CORSIM in the Traffic Software Integrated System, or TSIS, Version 4.32 (1999). A summary of some of the other relevant literature related to the rural median crossover is presented below in the following sections:

- Summaries of Design Guidance
- Problem Area Identification
- Improvement Measurement
- Operational Analysis


## SUMMARIES OF DESIGN GUIDANCE

NCHRP Report 279 - Intersection Channelization Design Guide, by Timothy R. Neuman. Transportation Research Board, National Research Council, Washington D.C. (1985).

The report provides principles and criteria for the applicability of channelization. Many examples are presented in detail.

NCHRP Report 375 - Median Intersection Design, by Douglas W. Harwood, Martin T. Pietrucha, Mark D. Woodldridge, Robert E. Brydia, and Kay Fitzpatrick. Transportation Research Board, National Research Council, Washington D.C. (1995).

This report focused on the selection of median widths for at-grade intersections on divided highways. It also presents some geometric and traffic control measures, including various median widths, left-turn lanes, offset left-turn lanes, indirect left-turn lanes, U-turn treatments, median acceleration lanes, and traffic control on the median roadway, etc.

NCHRP Synthesis 225 - Left-Turn Treatments at Intersections, by James L. Pline. Transportation Research Board, National Research Council, Washington D.C. (1996).

This report presents basic considerations for left turn treatments and summarizes design, signing, pavement marking, and signal considerations. Performance measures are presented as well as a discussion of special applications.

NCHRP Synthesis 281 - Operational Impacts of Median Width on Larger Vehicles, by Douglas W. Harwood and William D. Glauz. Transportation Research Board, National Research Council, Washington D.C. (2000).

Current median practices of the states are summarized. Operational and safety problems are then described. Alternative improvement techniques are then presented.

## PROBLEM AREA IDENTIFICATION

John C. Falcocchio, Robert M.Michel, Herbert S. Levinson, and Solomon Assefa, Priority Ranking of Problem Intersections in Brooklyn, N.Y., ITE Journal, Vol. 64, No. 5, May 1994.

The paper developed a problem ranking approach to judge a list of capital projects for improving traffic in North Brooklyn, N.Y. The process used delay and accident measures to determine the severity of problems at study locations. A severity score, to rank
problems, was based on the severity index and an intersection importance factor. These two components, in turn, were measured by traffic volume and stop delay or number of accidents.
N.M. Katamine, Various Volume Definitions with Conflicts at Unsignalized Intersections, Journal of Transportation Engineering, Vol. 126, No. 1, Jan. /Feb. 2000.

Through a traffic conflicts technique, this paper presents research carried out at 15 fourleg intersections in the capital of Jordan. By defining 13 types of volume, 11 types of conflicts, and 4 levels of severity grads, based upon field data collection and computers analysis, the author concluded:

- The effects of the approach volume on the correlation between volume and conflicts, in general, is made obvious when considering severity grade G4 (defined by the paper)
- Three basic volumes governing the correlation between volume and relevant conflicts were indicated by the corresponding definition of the paper.
- The use of some other volumes, defined by the paper as SP volume, XP volume, V-type volume, and CV volume, may provide misleading correlation with conflicts at intersections.


## IMPROVEMENT MEASUREMENT

Ahmed Essam Radwan, Kumares C. Sinha, and Harold L. Michael, Guidelines for Traffic Control at Isolated Intersections on High-Speed Rural Highways, Transportation Research Record 737, Transportation Research Board, National Academy of Science, Washington D.C. (1979).

Using field studies and traffic simulation, the paper presented warrants for selecting alternative traffic control at isolated intersections on high-speed rural highways. Twoway stop signs, pre-timed signals, semi-actuated signals, and fully actuated signals were evaluated over a range of traffic volume on major and minor approaches. The warrants were based on the criterion of minimum total annual cost, which include annual accident cost, delay cost, fuel cost, construction and maintenance cost of equipment, non-fuel operation cost, etc.

Daniel B. Fambro, John M. Mason, Jr., and Nancy Straub Cline, Intersection Channelization Guidelines for Longer and Wider Trucks, Transportation Research Record 1195, Transportation Research Board, National Research Council, Washington D.C. (1988).

Using a computer model and defining 2 singles (WB-50), 2 doubles (WB-70), and one triple (WB-100) as design vehicles, the paper generalized results into five topic areas: minimum turning radii, turning templates, cross-street width occupied, turning roadway width and channelization guidelines for longer and wider trucks. These guidelines include the minimum required curb radii to eliminate encroachment into either opposing or adjacent traffic lanes on the cross-street and the minimum required width of turning roadway.

James A. Bonneson, Patrick T. McCoy, and Jess E. Truby, Jr., Safety Improvements at Intersections on Rural Expressways: A Survey of State Departments of Transportation, Transportation Research Record 1385, Transportation Research Board, National Research Council, Washington D.C. (1993).

The state of the practice of measures that state highway departments used to improve traffic safety at intersections on rural expressways is described by the survey. According to the results of the survey, potential measurements include access control, traffic control measures, and geometric design measures. Most states indicated that an access opening is provided for each abutting parcel that cannot be served by other means, while median openings are provided only at intersections of the expressway and other public roads. As to traffic control measures, the responding states indicated that traffic signals were the most commonly applied measures. Other traffic control measures mentioned included specialized or enhanced signing and marking applications. Geometric design measures included alternative median widths, alternative left-turn bay, other left-turn treatments, interchanges, and some other geometric designs, such as adding a right-turn bay, lengthening the left-turn bay, adding a median acceleration lane, and adding a right-turn acceleration lane.

Joseph E. Hummer, Charles V. Zegeer, and Fred R. Hanscom, Effects of Turns by Larger Trucks at Urban Intersections. Transportation Research Record 1195, Transportation Research Board, National Research Council, Washington D.C. (1988).

The results showed that small curb radii, narrow lane widths, and narrow total street widths were among the geometric features associated with increased operational problems. Trailer length was found to be a most critical element to smooth operations than trailer width for the truck tested.

## OPERATIONAL ANALYSIS

Kay Fitzpatrick, Gaps Accepted at Stop-Controlled Intersections, Transportation Research Record 1303, Transportation Research Board, National Research Council, Washington D.C. (1991).

Data were used to determine intersection sight distance, capacity, queue length, and delay at unsignalized intersections. These data have also been used to determine the need for traffic signal, the capacity of a left-turn lane, warrants for left-turn signal phasing and storage lanes. In areas that experience significant truck traffic, gaps accepted by truck drivers should be considered. Six intersections were selected to collect field data. The Greenshield, Raff, and logit methods were selected to evaluate the gap data. The following conclusions were drawn for gap-acceptance by passenger car and by truck:

- Passenger car driver's 50 percent probability of accepting a gap was generalized as 6.5 sec . for both left and right turns and as 8.25 sec . for the 85 percent probability of accepting a gap at a moderate to high-volume intersection. A 10.5 sec . gap represents the 85 percent probability of accepting a gap at an intersection where the accepted gaps were influenced by low volume and the intersection geometry.
- Truck drivers' 50 percent probability of accepting a gap was generalized as 8.5 sec . In general, at a high-volume location, 85 percent of the truck drivers accepted a 10.0 sec . gap; at a low-volume location, 15.0 sec . was the accepted gap value.
- Some of the critical gap values determined at several of the intersections were influenced by geometric of traffic characteristics.

Michael Kyte, Chris Clemow, Naseer Mahfood, B. Kent Lall, and C. Jotin Khisty, Capacity and Delay
Characteristics of Two-way Stop-controlled Intersections, Transportation Research Record 1320, Transportation Research Board, National Research Council, Washington D.C. (1991).

Data were collected from a wide range of two-way stop-controlled intersections. Collected data included sight distance, upstream control and platoon characteristics, flow rate, delay, major-street gap, accepted and rejected gap data. It was concluded that:

- Average queue time increases as the subject approach flow rate increases.
- Average service time increases as the flow rate on the conflicting approaches increases.
- Minor-street capacity decreases as the major-street flow rate increases.
- Accepted gap are not constant, but very as a result of several factors, including queue time (inverse relationship), service time (slight inverse relationship), number of rejected gaps (inverse relationship), major street flow rate (inverse relationship), and directional movement of the subject vehicle.
- Service time and total delay increase as major-street flow rate increases
- The time in queue is not correlated to the major-street flow rate

A preliminary set of models to estimate capacity and delay was developed, including models to calculate capacity, total delay, queue time, and service time of minor-street.

Shane M. Velan and Michael Van Aerde, Gap Acceptance and Approach Capacity at Unsignalized Intersections, ITE Journal, Vol. 66, No.3, March 1996.

Using a microscopic gap acceptance model, under the defined base scenario of an opposed left turn from an unsignalized approach, several results were examined, including opposed approach capacity, size of critical gap, rate of temporal decay of the critical gap, and size of follow-up time. The paper concluded that:

- The opposing flow rate is determined primarily by the number of opposing lanes, their saturation flow rates, and the size of the critical gap and its rate of decay.
- The opposed approach capacity is controlled by the saturation flow rate of the opposed approach.

Wayne K. Kittelson and Mark. A. Vandehey, Delay Effects on Driver Gap Acceptance Characteristics at Two-way Stop-controlled Intersections, Transportation Research Record 1320, Transportation Research Board, National Research Council, Washington D.C. (1991).

This paper examined the 1985 Highway Capacity Manual definition of critical gap for two-way stopcontrolled intersections. A revision of the definition of critical gap considering both gap acceptances and gap rejections was presented first. The authors expressed it as "the median probability of accepting a gap of a given size" instead of "the median gap size that is accepted by drivers in a given situation" defined by HCM (1985). Some consequent conclusions were drawn:

- Critical gap is affected by the delay time. Drivers accept shorter gaps as front-of-queue delay increases.
- Any delay-based LOS criterion for TWSC intersections should incorporate lower delay thresholds than are used for signalized intersections, at least in the LOS D, E and F regions.
- The type of major-street conflict (same direction versus opposite direction) that is experienced also affects critical gap for minor-street left-turning vehicles. The directional distribution of major-street traffic can have a substantial effect on the capacity of this movement.


## APPENDIX 2: SUMMARY OF STATE AND LOCAL MEDIAN DESIGN PRACTICES, OPERATIONS AND SAFETY

Appendices A-F of National Cooperative Research Program Report 375: Median Intersection Design do not appear in the printed version of the report. These six appendices are available through a loan from the NCHRP. They are entitled:
A. Summary of Questionnaire Responses from State and Local Agencies
B. Field Observational Studies at Divided Highway Intersections
C. Evaluation of Accident Histories at Field Observational Sites
D. Evaluation of Statewide Accident Data for Divided Highway Intersections
E. Effect of Median Width on Traffic Operations at Signalized Intersections
F. Sight Distance Implications of Off-Setting Left-Turn Lanes at Divided Highway Intersections

Five of these six, Appendices A-E, are briefly summarized below. The purpose of this summary is to provide the reader with some of the relevant information in those appendices. The information here may also be useful so that one can determine whether to borrow those appendices from NCHRP.

## NCHRP 375 APPENDIX A - SUMMARY OF QUESTIONNAIRE RESPONSES FROM

## STATE AND LOCAL AGENCIES

## STATE HIGHWAY AGENCIES

43 responses of 50
Minimum Median Widths - Rural 3-64 ft. ( $41 \%$ greater than 30 ft. )

- Urban 1-30 ft. ( $57 \% 10 \mathrm{ft}$. or less)- 37 states

Desirable Median Widths - Rural 18-84 ft. ( $63 \%$ greater than 50 ft. )

- Urban 9-64 ft. ( $35 \%$ greater than 30 ft .) - 33 states

Maximum Median Widths - Rural 25-300 ft. (36\% greater than 100 ft )- 22 states

- Urban 16-101 ft. ( $71 \% 50 \mathrm{ft}$. or less)- 20 states

31 of 38 states consider the effect of median width on intersection operations when choosing the median width.
One state uses median widths of 150 ft . at intersections to create a dual intersection operation.
$50 \%$ of the reporting agencies indicated that storage considerations affect the width of the median.
Left-turning vehicles and safe separation are also considered in median width design.

## Special Provisions

Bicycles- 9 states
Pedestrians- 18 states
Left-turn Lanes-30 states
Indirect LT- 4 states
U-turns- 17 states
Other vehicle types- 6 states
10 state highway agencies intentionally design narrow medians to prevent storage of left-turning and crossroad vehicles in the median. 19 states have encountered operational or safety difficulties with these medians.

Medians were narrowed to increase capacity and operational efficiency, and to reduce the required right-of-way.
Vehicle overhang, inadequate U-turn space, and through-lane encroachment. Many states stated that the narrow medians were only a problem where left-turn lanes did not exist. Additional problems were lack of refuge areas and inability for expansion.

Signalized intersections at narrow medians cause problems with signal placement, pavement markings, left-turn treatments, and signal timing issues.

6 state agencies indicated that their policies account for the difference between signalized and unsignalized intersections.
$77 \%$ of the responding states indicated that they are satisfied with their current design policies. Many indicated that the median policies were too broad and needed to be more specific, in every aspect of the design. 8 states reported that changes are being considered to their median design policy.

## LOCAL HIGHWAY AGENCIES

## 19 responses of 51

7 use design policies in AASHTO Green Book
5 have created their own policy
5 use the state policy
9 have no formal design policy
(some overlap of answers)

Minimum widths- 1.5 to 50 ft .
Desirable widths- 8 to 60 ft .
Maximum widths-12 to 110 ft .
11 agencies make some estimation of queuing requirement for left turns in designing median widths.
$88 \%$ of the local agencies have guidelines regarding left-turn lanes
$42 \%$ consider bicyclists
$63 \%$ consider pedestrians
$63 \%$ consider U-turns
$36 \%$ consider driveway median openings
$52 \%$ consider larger vehicle types
2 agencies intentionally design narrow medians, these and 4 others have encountered operational and safety problems at medians that are too narrow.

5 local agencies reported operational and safety problems with wide medians.
The problems with wide medians involved left-turning vehicles blocking each other's sight lines and driver confusion when entering the median area to turn.

Nearly no local agencies differ their policies between signalized and unsignalized intersections.
$94 \%$ of the local agencies were content with their current guidelines for median width. 3 agencies were considering to their median policies.

## NCHRP 375 APPENDIX B - FIELD OBSERVATIONAL STUDIES AT DIVIDED HIGHWAY INTERSECTIONS

40 study sites
-20 rural four-leg intersections
-8 suburban four-leg unsignalized intersections
-6 suburban four-leg signalized intersections
-6 special feature intersections
2 with tapered offset LTL
1 with parallel offset LTL
2 with median acceleration lanes
2 three-leg intersections
Field studies states were California, Iowa, Illinois, Kansas, Maryland, Missouri, New Jersey, Pennsylvania, Texas, and West Virginia.

Major road was a divided highway and the minor road was an undivided highway or street in all cases.

## Characteristics of Intersections

## Rural Unsignalized Intersections

Uninterrupted flow on major road and STOP control on minor road approaches.

8 intersections had amber warning signals on the major and red signals on the minor road.
Major roads were four-lane divided highways with speed limit of 55 mph and minor road were two-lane undivided highways.

Median roadway control methods:

- 7 with STOP control
- 7 with YIELD control
- 6 with no control
- Rural special feature sites had no median roadway control

Median widths varied from 30 to 144 ft , and all were depressed, unpaved medians.
Turn Lanes:
Major road LT lanes: 16
Major road RT lanes: 11
Minor road LT lanes: 2
Minor road RT lanes: 2

## Suburban Unsignalized Intersections

All the suburban sites had major road uninterrupted flow and STOP control on the minor road approaches.
Geometric configurations were the same as for the rural unsignalized intersections.
The major road speed limits were 50 and 55 mph .
Median widths roadway control:

- 4 intersections with YIELD control
- 4 intersections with no control

Median was of both the depressed and raised variety.
Turn Lanes:
Major road LT lanes: 7
Major road RT lanes: 5
No minor road LT or RT

## Suburban Signalized Intersections

There were 2 or 3 through lanes per major approach, and 1 or 2 through lanes per crossroad approach.
Major road speed limits ranged from 45 to 55 mph .
Sites included raised and depressed medians.
Median widths ranged from 16 to 207 ft .
4 sites were signalized as a single intersection, with the other two sites designed as a double intersection with medians of over 200 ft .

Turn Lanes:
Major road LT lanes: 4
Major road RT lanes: 3
Minor road LT lanes: 1
Minor road RT lanes: 4

## Special Feature Intersections

3 rural unsignalized
3 suburban signalized
Specific special features are stated in the opening of this summary section.

## STUDY RESULTS

## Turning Behavior

Rural Unsignalized Intersections
Median widths less than 50 ft .- left turn movements tend to occur in front of one another.
Median widths greater than 50 ft - left turn movements occur behind one another (nearly all).

## Suburban Unsignalized Intersections

Median widths less than 50 ft .-nearly all LTs turned in front of one another.
Median widths greater than 50 ft .- LT turned in front also (LT channelization exists)
Undesirable Driving Behavior on Median Roadway
Side-by-side queuing on the median roadway by vehicles traveling the same direction Stopping at an angle on the median roadway
Encroachment on the through lanes of the major roadway.

## General Driving Movements and Undesired Behavior Frequency

Major road left/ Major road left same approach- 25.5\% of undesired maneuvers
Crossroad left/ Crossroad left same approach -10.2\%
Major road left/ Major road left opposite approach- 8.7\%
Crossroad left/ Major road left from right approach- 8.1\%
Crossroad through/ Crossroad left same approach-5.0\%
Crossroad left/ Cross through from same approach- 4.5\%
Major road left/ Crossroad left from left approach-4.3\%
Crossroad through/ Major road left from right approach- 4.1\%
$64.3 \%$ of undesired maneuvers involved vehicles traveling in the same direction $35.7 \%$ involved vehicles traveling in the opposite direction

Most common source of undesirable behavior appears to be competition for space between vehicles traveling in the same direction through the median.

## Median Width and Median Opening Length Effects

Rural Unsignalized Intersections:
Undesirable movements tend to decrease as median width increases- correlation is weak, though, and is barely significant at $90 \%$ confidence. Predominant undesirable movements is angle stopping.

Rates of undesired movements increase as the median opening length increases. The relationship is highly significant at $99.9 \%$ confidence. Therefore, median opening length should not be unnecessarily large.

There was a statistically significant inverse correlation between the slenderness ratio (ratio of median width to median opening) and the number of undesired movements. This information was not found to be helpful due to the correlations already established between the median width and the median opening individually.

Suburban Unsignalized Intersections
Undesirable movements tend to increase as median width increases, and the number of undesirable movements decrease as median opening increases, however it must be noted that the sample size is small. Angle stopping was the predominant undesired movement.

## Traffic Control Devices

11.6 to $42.7 \%$ of drivers in the median roadway were noncompliant with the STOP sign control, where 31 to $39 \%$ of drivers made rolling stops. No traffic conflicts resulted from these results.

Traffic control type was not found to diminish the effects of median width and median opening on driver behavior.

## Signalization Effects

Intersections that operated as a single unsignalized intersection had few undesirable movements, however, one of the state agencies had difficulty in loop placement and signal system design.

The two wide-median intersection sites that acted as two signalized intersections had troubles with both angle stopping and major road encroachment, mainly on the median roadway.

## Tapered and Parallel Offset Left-Turn Lanes

Undesirable movements at these sites involved backing in the through lanes to get to a missed turn lane and crossing of the gore area to enter a turn lane after entrance was missed, however, the frequency of these occurrences was low, and undesirable movements at these intersection in general were rare.

## Median Acceleration Lanes

The median acceleration lanes studied appeared to improve operations by reducing the need for cars to stop in the median roadway. The rates of undesirable movements were low at each of these study sites.

## NCHRP 375 APPENDIX C - EVALUATION OF ACCIDENT HISTORIES AT FIELD

## OBSERVATIONAL SITES

For the rural unsignalized intersections, no significant correlation was found between the median width and accident rates. The other intersection types had sample sizes to provide a meaningful result.

The suburban unsignalized intersection with the highest accident rates had a 26 ft . median, and it is suspected that the narrow median might be a contributing factor to the high accident rates.

Rear-end collisions were the most common at the suburban signalized intersections, however, the accident pattern is not related to the median area design.

The effects of trucks were not found to be very significant in either number of accidents or by encroaching onto the major roadway.

The samples were insufficient to provide evidence of a superior left-turn lane design.
The sample of wrong-way accidents was too small to determine the effects of median width on wrong-way accidents.

## NCHRP 375 APPENDIX D - EVALUATION OF STATEWIDE ACCIDENT DATA FOR

 DIVIDED HIGHWAY INTERSECTIONSCalifornia database used for the analysis.
Poison and log-normal regression analyses were used to analyze the accident data from the database on about 6800 intersections on divided highways.

At rural four-leg unsignalized intersections, it was determined that accident frequency decreases as median width increases, with the result found to be statistically significant.

No statistically significant relationship was found to exist between accident frequency and median width at three-leg unsignalized intersections.

At urban/suburban four-leg signalized intersections, accident frequency was found to increase over median widths for 14 to 80 ft ., with the result being statistically significant.

At three-leg urban/suburban intersections, accident frequency was found to increase with increasing median width, with the result being statistically significant.

## NCHRP 375 APPENDIX E - EFFECT OF MEDIAN WIDTH ON TRAFFIC

## OPERATIONS AT SIGNALIZED INTERSECTIONS

There are least two possibilities for signalization of an intersection at a divided roadway, wheher a single intersection signalization design or a diamond intersection signalization design. The former appears to be more appropriate for narrow medians, while the latter appears to be more feasible for wide medians.

At single intersection signalizations, delay increases as median width increases.
The breakdown points occur at the following widths to determine whether to use single or diamond signal design:

- High Volumes: 98 to 148 ft .
- Moderate Volumes: 200 to 300 ft .
- General Case: 100 ft or less for single signal 150 ft . or more for diamond

However, the scenarios presented in the section are not likely to match design situations, due to forecasting inaccuracies, and so the designer is cautioned to use their judgment.

## APPENDIX 3: Crossovers of potential Concern Identified by MoDOT Districts

Each of the ten MoDOT Districts were asked to identify type 2 median crossovers with congestion for potential study. The responses to this request are shown in this appendix in the following tables.

Table C-1: Crossovers of Concern to MoDOT Districts

Table C-2: District 5 Top Crossover Accident Locations without Deceleration Lanes
Table C-3: District 5 Top Crossover Accident Locations with Deceleration Lanes
Table C-4 : District 5 Crossover Accidents

Table C-1: Crossovers of Concern to MoDOT Districts

| District | County | City | Location | Log Mile | Speed Limit | Contact | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Caldwell |  | Rte. 36 \& B36/P |  |  | Jody Carlson 816-384-2452 |  |
| 2 | Saline | Marshall | Rte. 65 \& B65 South |  |  | Bob Bradley 660-385-8626 | not typical type2 |
|  | Linn | Meadville | Rte. 36 \& Rte. 139/W |  |  |  | not typical type2 |
|  | Linn | Laclede | Rte. 36 \& Rte. 139/5 |  |  |  | not typical type2 |
| 3 | Lincoln | Troy | US 61 \& North Lincoln Drive | 16.00 |  | Kevin James 573-248-2418 |  |
|  | Lincoln | Troy | US 61 \& South Lincoln Drive | 19.06 |  |  |  |
|  | Lincoln | Moscow Mills | US 61 \& Tropicana Village Road | 20.20 |  |  |  |
|  | Lincoln | Moscow Mills | US 61 \& Rte. C | 20.87 |  |  |  |
|  | Lincoln | $\begin{gathered} \text { Moscow } \\ \text { Mills } \end{gathered}$ | US 61 \& Main Street | 21.27 |  |  |  |
|  | Marion | Palmyra | US 61 \& Main Cross | 10.40 |  |  |  |
|  | Marion | Palmyra | US $61 \&$ Ross Street | 10.75 |  |  |  |
|  | Ralls | Hannibal | US 61 \& Warren Barrett/Industrial Drive | 0.58 |  |  |  |
|  | Ralls | New London | US $61 \&$ Rte. A | 7.02 |  |  |  |
| 4 | Cass |  | Rte. 71 \& Rte. T |  | 70 | Marisela Guillen 816-889-6423 |  |
|  | Cass |  | Rte. 71 \& 307th Street |  | 70 |  |  |
|  | Cass |  | Rte. 7 \& Rte. TT |  | 70 |  |  |
|  | ? |  | Rte. 152 \& Shoal Creek |  |  | Tony Moore 816-889-6426 |  |
| 5 |  |  | See Tables C-2 and C-3 |  |  | Jacob Ray 573-526-6880 |  |
| 6 |  |  | None Submitted |  |  |  |  |
| 7 | Bates |  | US $71 \&$ MO 52 east |  |  | Daryl Weinkein 417-629-3322 | priority 1 |
|  | Barton |  | US 71 \& MO 126 |  |  |  | priority 2 |
|  | Jasper |  | MO 66 \& Black Cat Road |  |  |  | priority 3 |
|  | Jasper |  | MO 66 \& Central City Road |  |  |  | priority 5 |
|  | Newton |  | US 71 \& MO D |  |  |  | priority 4 |

Table C-1 (continued): Crossovers of Concern to MoDOT Districts

| District | County | City | Location | Log Mile | Speed Limit | Contact | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 8 | Greene |  | Rte. 13 \& Rte. O |  | 65 | Leo Cologna 417-895-7639 | meets signal warrants |
|  | Greene |  | Rte. 160 \& Farm Road 157 |  | 60 |  | meets signal warrants |
|  | Greene |  | Rte. 13 \& Rte. WW |  | 65 |  |  |
|  | Greene |  | Rte. 60 \& Rte. 125 |  | 60 |  | signalized |
|  | Webster |  | Rte. 60 \& Rte. C/K |  | 65 |  | meets signal warrants |
|  | Webster | Seymour | Rte. 60 \&Old Rte. 60 |  | 65 |  | meets signal warrants |
|  | Polk |  | Rte. 13 \& Rte. U/Y |  | 65 |  |  |
| 9 |  |  | None Submitted |  |  |  |  |
| 10 |  |  | None Submitted |  |  |  |  |

Table C-2: District 5 Top Crossover Accident Locations without Deceleration Lanes

| Rank | County | Route | At | Log Point | 1994-98 Accidents |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Callaway | 54 | FF / North Outer Rd | 29.64 | 20 |
| 2 | Cole | 54 | Goller Rd | 13.61 | 15 |
| 3 | Cole | 54 | Old Bass / Brown Rd | 6.20 | 13 |
| 4 | Cole | 54 | Rickman Rd | 16.37 | 12 |
| 5 | Cole | 54 | Honeycreek Rd / Heritage Hwy | 10.09 | 12 |
| 6 | Pettis | 50 | H / HH | 13.32 | 12 |
| 7 | Cole | 54 | Cassidy Road | 10.96 | 11 |
| 8 | Callaway | 54 | CR 210 / CR 114 | 26.62 | 9 |
| 9 | Cole | 50/63 | Eastwood Dr / LePage Rd | 4.36 | 9 |
| 10 | Callaway | 54 | CR 220 | 28.30 | 8 |
| 11 | Pettis | 50 | Pleasant Green Rd | 4.48 | 8 |
| 12 | Cole | 54 | Monticello Rd | 13.01 | 7 |
| 13 | Cole | 54 | D | 9.25 | 7 |
| 14 | Cole | 54 | Brazito Rd | 7.62 | 7 |
| 15 | Miller | 54 | CR 52-18 | 8.57 | 7 |

Table C-3: District 5 Top Crossover Accident Locations with Deceleration Lanes

| Rank | County | Route | At | Log Point | $\begin{gathered} \hline \text { 1994-98 } \\ \text { Accidents } \end{gathered}$ | Current Conditions |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Callaway | 54 | South Outer Rd (McStop) | 29.09 | 52 | Signal, Decel Lanes (installed 5/6/94) |
| 2 | Cole | 54 | Idlewood | 15.78 | 45 | Decel Lanes (installed Oct. 1996), Future Interchange |
| 3 | Miller | 54 | Bus 54 / W | 3.69 | 40 | Decel, Accel Lanes (installed Fall 1998) |
| 4 | Pettis | 50 | MM | 10.70 | 39 | Decel Lanes |
| 5 | Boone | 63 | Hinton / Calvert Hill Rd | 13.40 | 30 | Decel Lanes (installed Fall 1997) |
| 6 | Camden | 54 | A | 23.86 | 29 | Decel Lanes (installed approx. 1997) |
| 7 | Cole | 54 | CC | 14.51 | 25 | Decel Lanes (installed Oct. 1996) |
| 8 | Miller | 54 | FF (Opies) | 16.90 | 25 | Decel Lanes (installed approx. 1996) |
| 9 | Cole | 50/63 | Cityview Drive | 4.52 | 24 | Decel Lanes |
| 10 | Pettis | 50 | MO 127 | 3.98 | 22 | Decel Lanes |
| 11 | Callaway | 54 | FF / North Outer Rd | 29.64 | 20 | Flasher |
| 12 | Camden | 54 | $\begin{aligned} & \hline \text { Valley Dr / CR 54- } \\ & 68 \end{aligned}$ | 22.86 | 20 | Decel Lanes |
| 13 | Cole | 54 | E / Pleasant Hill Rd | 7.24 | 20 | Decel Lanes (installed Oct. 1996) |
| 14 | Boone | 63 | 163 | 28.38 | 19 | Decel Lanes (installed Oct. 1996) |
| 15 | Cole | 54 | Buffalo Rd / Heritage Hwy | 12.41 | 19 | Decel Lanes (installed Oct. 1996) |
| 16 | Boone | 63 | AB / Deer Park Rd | 28.89 | 16 | Decel Lanes (installed 1996) |
| 17 | Boone | 63 | H / Log Providence Rd | 30.90 | 16 | Flasher, Decel Lanes (installed 1996) |
| 18 | Cole | 54 | Goller Rd | 13.61 | 15 |  |
| 19 | Callaway | 54 | T | 34.76 | 14 | Decel Lanes (installed approx 1996) |
| 20 | Boone | 63 | $\begin{gathered} \hline \text { Dripping Springs } \\ \text { Rd } \end{gathered}$ | 11.18 | 13 | Decel Lanes |
| 21 | Boone | 63 | Ponderosa St / <br> Huggard Rd | 26.84 | 13 | Decel Lanes (installed approx 1996) |

Table C-3 (continued) : District 5 Top Crossover Accident Locations with Deceleration Lanes

| Rank | County | Route | At | Log Point | $\mathbf{1 9 9 4 - 9 8}$ <br> Accidents | Current Conditions |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 22 | Cole | 54 | Old Bass / Brown <br> Rd | 6.20 | 13 |  |
| 23 | Miller | 54 | MM / CR 54-70 | 19.86 | 13 | Decel Lanes (installed approx 1996) |
| 24 | Cole | 54 | Rickman Rd | 16.37 | 12 | 12 |
| 25 | Cole | 54 | Honeycreek Rd $/$ <br> Heritage Hwy | 10.09 | 12 |  |
| 26 | Pettis | 65 | H / HH | 13.32 | 12 |  |
| 27 | Cole | 54 | Cassidy Road | 10.96 | 11 | Decel Lanes |
| 28 | Miller | 54 | CR 54-66 | 17.87 | 11 | Decel Lanes |
| 29 | Boone | 63 | MO $124(S)$ | 8.60 | 10 |  |

## Table C-4 : District 5 Crossover Accidents



| BOONE | LIBERTY LANE | 63 | 35.68 | 2 |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| BOONE | PETERSON LN / RAY FORSEE RD | 63 | 35.91 | 3 |  |  |  |  |  |
| BOONE | $\begin{aligned} & \text { BLYTHE RD / GILPIN } \\ & \text { RD } \end{aligned}$ | 63 | 37.17 | 0 |  |  |  |  |  |
| BOONE | A / GILMORE LANE | 63 | 37.92 | 2 | 160 | 100 | 230 | 260 | Decel Lanes installed approx. 1996 |
| BOONE | ZUMWALT ROAD | 63 | 38.97 | 0 |  |  |  |  |  |
| BOONE | WESTBROOK DR / MT. PLEASANT | 63 | 40.19 | 1 | 0 | 0 | 160 | 760 |  |
| BOONE | CLAYSVILLE RD | 63 | 42.49 | 0 |  |  |  |  |  |
| BOONE | HARTMAN RD | 63 | 43.01 | 1 |  |  |  |  |  |
| CALLAWAY | CR 2002 | 54 | 38.26 | 4 |  |  |  |  |  |
| CALLAWAY | CR 1048 | 54 | 37.30 | 0 |  |  |  |  |  |
| CALLAWAY | T | 54 | 34.76 | 14 | 220 | 260 | 180 | 270 | Decel Lanes installed approx. 1996 |
| CALLAWAY | CR 158 | 54 | 33.75 | 0 |  |  |  |  |  |
| CALLAWAY | CR 147 | 54 | 31.78 | 1 | 220 | 240 | 220 | 280 |  |
| CALLAWAY | CR 240 / CR 148 | 54 | 30.52 | 2 |  |  |  |  |  |
| CALLAWAY | FF / NORTH OUTER RD | 54 | 29.64 | 20 |  |  |  |  | Flasher |
| CALLAWAY | $\begin{gathered} \text { TACO BELL } \\ \text { CROSSOVER } \\ \hline \end{gathered}$ | 54 | 29.45 | 6 |  |  |  |  |  |
| CALLAWAY | SOUTH OUTER RD(McStop) | 54 | 29.09 | 52 | 260 | 420 | 240 | 240 | SIGNAL EB Rt Turn-180' <br> Taper, 210' Lane; WB Rt <br> Turn-820' Lane, Signal <br> installed 5/6/94 |
| CALLAWAY | CR 220 | 54 | 28.30 | 8 |  |  |  |  |  |
| CALLAWAY | CR 209 / CR 110 | 54 | 27.33 | 2 |  |  |  |  |  |
| CALLAWAY | CROSSOVER | 54 | 27.00 | 3 |  |  |  |  |  |
| CALLAWAY | CR 210 / CR 114 | 54 | 26.62 | 9 |  |  |  |  |  |
| CALLAWAY | CR 201 | 54 | 26.04 | 3 |  |  |  |  |  |
| CALLAWAY | CR 200 | 54 | 24.82 | 2 | 80 | 130 | 0 | 0 |  |
| CALLAWAY | HH | 54 | 24.23 | 5 | 250 | 260 | 120 | 260 | Flasher, Decel Lanes |


|  |  |  |  |  |  |  |  |  | installed May 96 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CALLAWAY | $\begin{aligned} & \hline \text { CR } 204 \text { / ATKINSON } \\ & \text { RD } \end{aligned}$ | 54 | 23.33 | 9 | 180 | 630 | 140 | 280 | SIGNAL EB Rt Turn-200' Taper, 670' Lane, Signal installed 1/4/2000 |
| CALLAWAY | $\begin{gathered} \text { CR } 306 \text { / OLD } \\ \text { JEFFERSON CITY RD } \end{gathered}$ | 54 | 21.25 | 3 | 80 | 140 | 80 | 140 |  |
| CALLAWAY | CR 318 | 54 | 17.92 | 4 | 90 | 120 | 90 | 120 |  |
| CALLAWAY | BB / CR 328 | 54 | 15.85 | 5 | 160 | 300 | 200 | 300 | Decel Lanes installed approx. 1996 |
| CALLAWAY | CR 338 | 54 | 14.61 | 1 | 80 | 140 | 80 | 140 |  |
| CALLAWAY | CR 348 | 54 | 12.99 | 0 | 100 | 140 | 100 | 140 |  |
| CALLAWAY | CR 399 / CR 397 | 63 | 0.31 | 1 |  |  |  |  |  |
| CALLAWAY | CR 394 | 63 | 0.87 | 0 | 150 | 180 | 150 | 210 | Decel Lanes installed approx. 1996 |
| CALLAWAY | ROY WAYNE RD | 63 | 1.55 | 5 |  |  |  |  |  |
| CALLAWAY | RENZ RD / NICKEL | 63 | 3.36 | 1 | 250 | 140 | 120 | 220 | Decel Lanes installed approx. 1996 |
| CAMDEN | CROSS CREEK <br> ENTRANCE | 54 | 21.97 | 1 |  |  |  |  |  |
| CAMDEN | CR 54-72 | 54 | 22.24 | 8 | 160 | 320 | 120 | 400 |  |
| CAMDEN | V | 54 | 22.54 | 1 | 240 | 280 | 120 | 420 |  |
| CAMDEN | VALLEY DR / CR 54-68 | 54 | 22.86 | 20 | 120 | 220 | 120 | 360 |  |
| CAMDEN | A | 54 | 23.86 | 29 | 240 | 280 | 120 | 260 |  |
| CAMDEN | LAKE ROAD 54-59A | 54 | 24.34 | 3 | 0 | 0 | 120 | 460 |  |
| COLE | EXPRESSVIEW DR | 50/63 | 3.48 | 0 |  |  |  |  |  |
| COLE | $\begin{aligned} & \hline \text { ROLLING HILLS RD / } \\ & \text { SCHOTT RD } \end{aligned}$ | 50/63 | 3.66 | 6 |  |  |  |  |  |
| COLE | $\begin{aligned} & \text { EASTWOOD DR / } \\ & \text { LEPAGE RD } \end{aligned}$ | 50/63 | 4.36 | 9 |  |  |  |  |  |
| COLE | CITYVIEW DR | 50/63 | 4.52 | 24 | 120 | 160 | 240 | 260 | WB Rt Turn-180' Taper, $180^{\prime}$ Lane |
| COLE | CROSSOVER | 50/63 | 5.08 | 0 | 100 | 160 | 120 | 850 | WB Rt Turn-160' Taper, 160' Lane |
| COLE | LIBERTY / SHAMROCK RD | 50/63 | 6.01 | 5 |  |  |  |  |  |


| COLE | LISLETOWN ROAD | 50/63 | 9.56 | 0 |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| COLE | CROSSOVER | 50/63 | 10.92 | 0 |  |  |  |  |  |
| COLE | RICKMAN RD | 54 | 16.37 | 12 |  |  |  |  |  |
| COLE | IDLEWOOD / <br> SOUTHWOOD HILLS | 54 | 15.78 | 45 | 240 | 340 | 270 | 310 | Decel Lanes installed Oct 1996 |
| COLE | ROCKPORT HILLS RD | 54 | 15.59 | 6 |  |  |  |  |  |
| COLE | MISSOURI FURNITURE | 54 | 15.23 | 1 |  |  |  |  |  |
| COLE | DULLE RESIDENCE | 54 | 14.90 | 2 |  |  |  |  |  |
| COLE | CC | 54 | 14.51 | 25 | 0 | 0 | 120 | 140 | Decel Lanes installed Oct 1996 |
| COLE | SHEPHERD HILLS RD | 54 | 14.26 | 7 | 180 | 300 | 0 | 0 | Decel Lanes installed Oct 1996 |
| COLE | GOLLER RD | 54 | 13.61 | 15 |  |  |  |  |  |
| COLE | MONTICELLO RD | 54 | 13.01 | 7 |  |  |  |  |  |
| COLE | TWIN BRIDGES | 54 | 12.67 | 0 |  |  |  |  |  |
| COLE | BUFFALO RD / HERITAGE HWY | 54 | 12.41 | 19 | 120 | 360 | 240 | 260 | Decel Lanes installed Oct 1996 |
| COLE | QUARRY RD | 54 | 11.41 | 0 |  |  |  |  |  |
| COLE | CASSIDY ROAD | 54 | 10.96 | 11 |  |  |  |  |  |
| COLE | CROSSOVER | 54 | 10.65 | 0 |  |  |  |  |  |
| COLE | TONIA LN / PESCHANG PARKWAY | 54 | 10.34 | 0 |  |  |  |  |  |
| COLE | HONEYCREEK RD / HERITAGE HWY | 54 | 10.09 | 12 |  |  |  |  |  |
| COLE | NEW CHURCH RD | 54 | 9.50 | 0 |  |  |  |  |  |
| COLE | D | 54 | 9.25 | 7 |  |  |  |  |  |
| COLE | OLD RIDGE RD | 54 | 8.72 | 4 |  |  |  |  |  |
| COLE | PLEASANT HILL RD | 54 | 8.09 | 0 |  |  |  |  |  |
| COLE | BRAZITO RD | 54 | 7.62 | 7 |  |  |  |  |  |
| COLE | E / PLEASANT HILL RD | 54 | 7.24 | 20 | 240 | 410 | 120 | 360 | Decel Lanes installed Oct 1996 |


| COLE | GRAY RD | 54 | 6.79 | 5 |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| COLE | $\begin{gathered} \hline \text { OLD BASS / BROWN } \\ \text { RD } \end{gathered}$ | 54 | 6.20 | 13 |  |  |  |  |  |
| COLE | FALL HILL RD | 54 | 5.78 | 4 |  |  |  |  |  |
| COLE | SANDY FORK / QUAIL RD | 54 | 4.92 | 3 |  |  |  |  |  |
| COLE | UNITED RD / FARM VIEW RD | 54 | 4.11 | 3 |  |  |  |  |  |
| COLE | CLARK FORK/ HICKORY HILL | 54 | 3.02 | 5 |  |  |  |  |  |
| COLE | PENNY HOLLOW LANE | 54 | 2.49 | 1 |  |  |  |  |  |
| MILLER | AA | 54 | 22.96 | 0 | 120 | 200 | 120 | 250 | Decel Lanes installed approx. 1996 |
| MILLER | CR 54-74 | 54 | 21.38 | 0 | 0 | 0 | 120 | 170 |  |
| MILLER | CR 54-72 | 54 | 20.48 | 2 | 0 | 0 | 120 | 170 |  |
| MILLER | MM / CR 54-70 | 54 | 19.86 | 13 | 120 | 200 | 120 | 200 | EB Rt Turn-200' Lane, Decel Lanes installed approx. 1996 |
| MILLER | CR 54-68 | 54 | 19.16 | 2 | 0 | 0 | 120 | 170 |  |
| MILLER | CR 54-66 | 54 | 17.87 | 11 | 0 | 0 | 120 | 170 |  |
| MILLER | FF(Opies) | 54 | 16.90 | 25 | 120 | 540 | 120 | 540 | Decel Lanes installed approx. 1996 |
| MILLER | CR 54-64 (CAVE DRIVE) | 54 | 10.44 | 2 | 240 | 120 | 240 | 120 | Decel Lanes installed approx. 1996 |
| MILLER | CROSSOVER | 54 | 9.63 | 0 |  |  |  |  |  |
| MILLER | CR 52-18 | 54 | 8.57 | 7 |  |  |  |  |  |
| MILLER | CR 54-60 | 54 | 7.71 | 3 |  |  |  |  |  |
| MILLER | CROSSOVER (ALLEN RD) | 54 | 6.69 | 0 |  |  |  |  |  |
| MILLER | $\begin{gathered} \text { CR 54-56 (HOWSER } \\ \text { ROAD) } \\ \hline \end{gathered}$ | 54 | 6.47 | 1 |  |  |  |  |  |
| MILLER | WALNUT GROVE RD | 54 | 5.93 | 1 |  |  |  |  |  |
| MILLER | V | 54 | 5.29 | 4 |  |  |  |  |  |
| MILLER | CR 54-54 | 54 | 4.92 | 5 |  |  |  |  |  |


| MILLER | CROSSOVER | 54 | 4.13 | 0 |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MILLER | CR 54-52 / BUS 54 / W | 54 | 3.69 | 40 | 180 | 480 | 200 | 400 | Acceleration Lane-500' Taper,850' Lane; WB Rt Turn-400' Lane, Decel \& Accel Lanes installed Fall 1998 |
| PETTIS | FF / THOMPSON RD | 50 | 0.00 | 7 | 130 | 140 | 170 | 110 |  |
| PETTIS | DUTCH KOUNTRY MARKET RD | 50 | 0.32 | 1 |  |  |  |  |  |
| PETTIS | KNOB NOSTER RD | 50 | 0.94 | 0 |  |  |  |  |  |
| PETTIS | CROSSOVER | 50 | 1.47 | 1 |  |  |  |  |  |
| PETTIS | ALLEN RD | 50 | 1.96 | 0 |  |  |  |  |  |
| PETTIS | CROSSOVER | 50 | 2.68 | 0 |  |  |  |  |  |
| PETTIS | OLD US HIGHWAY 50 | 50 | 3.22 | 1 |  |  |  |  |  |
| PETTIS | MO 127 | 50 | 3.98 | 22 | 260 | 260 | 260 | 260 |  |
| PETTIS | PLEASANT GREEN RD | 50 | 4.48 | 8 |  |  |  |  |  |
| PETTIS | CROSSOVER | 50 | 5.05 | 0 |  |  |  |  |  |
| PETTIS | CRYSTAL SPRINGS <br> RD | 50 | 5.47 | 0 |  |  |  |  |  |
| PETTIS | NFO RD | 50 | 6.19 | 0 |  |  |  |  |  |
| PETTIS | CHEVALIER RD | 50 | 6.48 | 4 |  |  |  |  |  |
| PETTIS | $\begin{gathered} \text { BUCKLEY / BUCKEYE } \\ \text { RD } \end{gathered}$ | 50 | 6.84 | 0 |  |  |  |  |  |
| PETTIS | CROSSOVER | 50 | 7.47 | 1 |  |  |  |  |  |
| PETTIS | HITAFFER RD | 50 | 7.98 | 0 |  |  |  |  |  |
| PETTIS | T / DRESDEN RD | 50 | 8.85 | 4 | 240 | 260 | 300 | 270 |  |
| PETTIS | ROADSIDE PARK RD | 50 | 9.15 | 0 | 240 | 0 | 300 | 260 |  |
| PETTIS | MM / SACHE LN | 50 | 10.70 | 39 | 280 | 260 | 280 | 260 |  |
| PETTIS | BRYDEN CHIROPRACTIC CROSSOVER | 50 | 11.15 | 1 |  |  |  |  |  |
| PETTIS | HOWARD FARMS CROSSOVER | 50 | 11.53 | 3 | 250 | 250 | 340 | 240 |  |


| PETTIS | CROSSOVER | 65 | 0.02 | 0 |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PETTIS | CC / SPRING GARDEN RD | 65 | 0.57 | 1 |  |  |  |  |  |
| PETTIS | CROSSOVER | 65 | 0.72 | 0 |  |  |  |  |  |
| PETTIS | WILDWOOD RD | 65 | 1.31 | 0 |  |  |  |  |  |
| PETTIS | CROSSOVER | 65 | 1.96 | 0 |  |  |  |  |  |
| PETTIS | BB / TRICKUM RD | 65 | 2.06 | 0 |  |  |  |  |  |
| PETTIS | CROSSOVER | 65 | 2.55 | 0 |  |  |  |  |  |
| PETTIS | CROSSOVER | 65 | 3.07 | 0 |  |  |  |  |  |
| PETTIS | DEER PARK RD | 65 | 3.46 | 0 |  |  |  |  |  |
| PETTIS | HOUSTON RD | 65 | 3.64 | 2 |  |  |  |  |  |
| PETTIS | CROSSOVER | 65 | 3.92 | 0 |  |  |  |  |  |
| PETTIS | CROSSOVER | 65 | 4.36 | 0 |  |  |  |  |  |
| PETTIS | SHANNON DRIVE | 65 | 4.76 | 0 |  |  |  |  |  |
| PETTIS | D / J | 65 | 5.22 | 4 |  |  |  |  |  |
| PETTIS | ABREY RD | 65 | 5.78 | 1 |  |  |  |  |  |
| PETTIS | CROSSOVER | 65 | 6.21 | 1 |  |  |  |  |  |
| PETTIS | $\begin{gathered} \text { KEMP / HUGHESVILLE } \\ \text { RD } \end{gathered}$ | 65 | 6.47 | 0 |  |  |  |  |  |
| PETTIS | CROSSOVER | 65 | 6.88 | 3 |  |  |  |  |  |
| PETTIS | CLAYCOMB RD | 65 | 7.22 | 2 |  |  |  |  |  |
| PETTIS | THORNLEIGH RD | 65 | 7.85 | 0 |  |  |  |  |  |
| PETTIS | CROSSOVER | 65 | 8.63 | 0 |  |  |  |  |  |
| PETTIS | SMEISER RD | 65 | 9.47 | 0 |  |  |  |  |  |
| PETTIS | BOTHWELL PARK RD | 65 | 10.29 | 1 |  |  |  |  |  |
| PETTIS | MT. HERMAN RD | 65 | 11.15 | 1 |  |  |  |  |  |
| PETTIS | RUNGE CROSSOVER | 65 | 11.31 | 0 | 160 | 150 | 180 | 110 |  |
| PETTIS | SWOPE RD | 65 | 12.40 | 2 |  |  |  |  |  |
| PETTIS | CROSSOVER | 65 | 13.02 | 2 |  |  |  |  |  |
| PETTIS | H / HH | 65 | 13.32 | 12 |  |  |  |  |  |


| PETTIS | CROSSOVER | 65 | 13.70 | 2 |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PETTIS | CROSSOVER | 65 | 19.50 | 1 |  |  |  |  |  |
| PETTIS | CROSSOVER | 65 | 20.06 | 1 |  |  |  |  |  |
| PETTIS | HALL RD | 65 | 20.80 | 1 |  |  |  |  |  |
| PETTIS | RYAN RD | 65 | 21.07 | 2 |  |  |  |  |  |
| PETTIS | $\begin{array}{\|c} \text { MARIGOLD RD / BALL } \\ \text { RD } \end{array}$ | 65 | 21.58 | 1 |  |  |  |  |  |
| PETTIS | F | 65 | 22.20 | 5 | 200 | 120 | 180 | 120 |  |
| PETTIS | GLAZEBROOK RD | 65 | 22.68 | 0 |  |  |  |  |  |
| PETTIS | WESTMORELAND | 65 | 23.64 | 0 |  |  |  |  |  |
| PETTIS | SMASAL | 65 | 24.48 | 0 |  |  |  |  |  |
| PETTIS | V / MALTEBERGER | 65 | 25.48 | 5 | 160 | 120 | 120 | 140 |  |
| PETTIS | MATHER | 65 | 26.48 | 1 |  |  |  |  |  |
| PETTIS | MANILA | 65 | 27.48 | 1 |  |  |  |  |  |
| PETTIS | MO 52 | 65 | 28.47 | 9 | 210 | 100 | 240 | 320 |  |

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